CAES Modeling



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Matt Kirk, Mark Grubelich, Steve Webb, Scott Broome SAND 2010-6940C

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Specific and existing problems, interests, needs



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- 1-Potential Microbial and Chemical Impact of CAES in a Sandstone, M. Kirk
- 2-Assessment of Ignition/Explosion Potential in a Depleted Hydrocarbon Reservoir from Air Cycling Associated with CAES, M. Grubelich
- 3-Flow Analysis Parametric Study: S. Webb
- 4-Material Degradation (T-M-C-H effects) Due to Cyclic Loading, SJ Bauer and ST Broome

Started November 2009



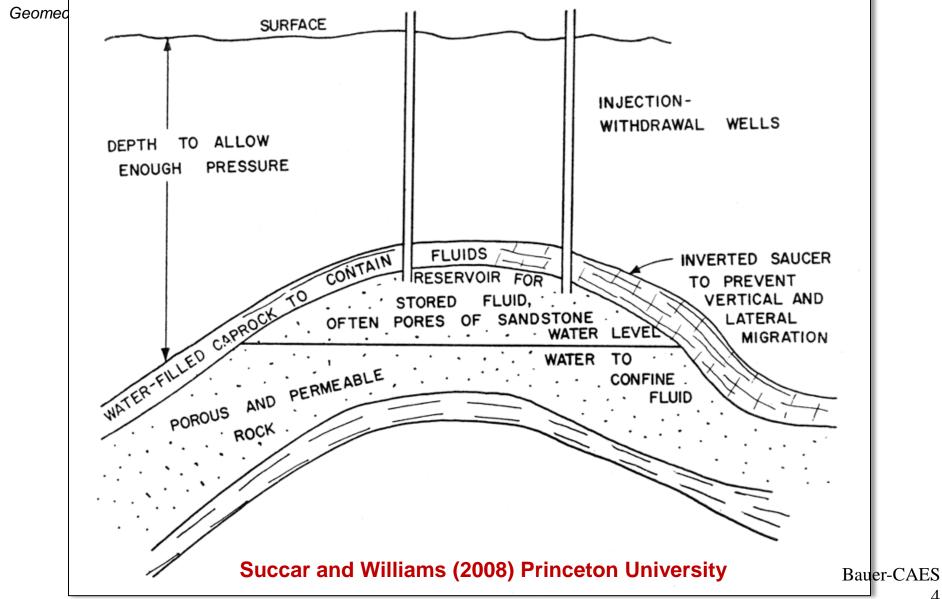
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Potential Microbial and Chemical Impact of CAES in a Sandstone

Matthew Kirk Geochemistry Department

Compressed Air Energy Storage

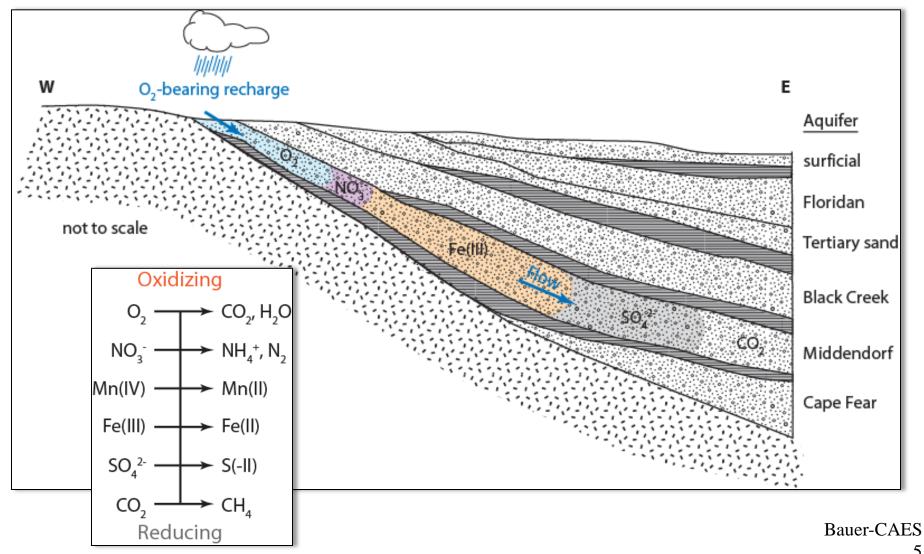




Groundwater Microbiology



Example: Middendorf coastal plain aquifer, South Carolina



Conclusions: Potential Microbial and Chemical Impact of CAES in a Sandstone

- Sandstone evaluated in a reducing environment
- Microbial Fe(II) and Mn(II) oxidation will become favorable
- Pyrite oxidation could lead to considerable changes in pH, salinity, and mineralogy
- Microbiology and mineralogy changes would impact porosity

Considerations for Explosion Potential for CAES in a Depleted Natural Gas Reservoir



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Mark Grubelich Geothermal Energy



Results & Conclusions: Mitigation & Safety



- Purge reservoir before use
- Low pressure air cycling below UFL to remove gas (~90 psi)
- In-situ gas monitor
- Never draw down air below the LFL (370 psi)
- Insure no surface breach if ignition occurs (sufficient overburden)
- Monitor NG content entering surface equipment
- Further study required
 - Buoyancy issues, etc.



CAES Borehole Study: Steve Webb



- Objective
 - Look at Flow in Individual Boreholes
 - Simple 2-d Models
 - Estimate Number of Boreholes and CAES Footprint
- Assumptions
 - Representative Borehole/Formation Geometry
 - Include Two-Phase Behavior
 - Capillary Pressure and Relative Permeability
 - Bubble Formation
 - Air Injection and Withdrawal 10 Weekly Cycles

Conclusions

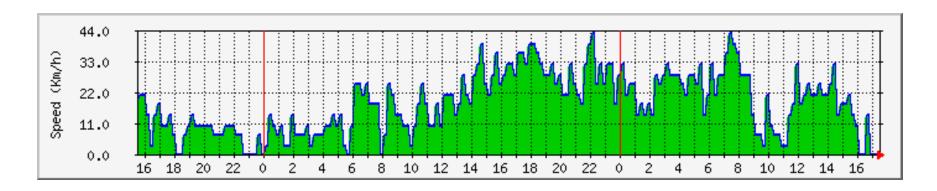


- Permeability Variation Much More Important than Porosity Variation
- Procedure Can Quantify Differences Between Various Sets of Formation Parameters
 - Borehole Spacing, Number of Boreholes
- Borehole Arrays Will Be Investigated in the Future



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Material Degradation (T-M-C-H effects) Due to Cyclic Loading SJ Bauer and ST Broome



Hourly fluctuations in wind speed could translate to frequent pressurization/depressurizations of salt caverns

Concluding Comments



- Preliminary cyclic tests completed on salt
- Change in volume strain observed
- Young's Modulus changes observed
- **Acoustic emissions detected**
- Cracks observed in thick sections
- Results consistent with previous work
- Implication that cyclic loading caused cracking at low differential stresses

Summary/Conclusions



- 1- Sandstone in a reducing environment could effect biologic and mineralogic changes that could lead to changes in porosity and permeability
- 2-Recommendations given for mitigation of potential use of a natural gas reservoir for CAES
- 3- Permeability variation much more important than porosity variation; procedure can help determine borehole spacing, number of boreholes (CO\$T)
- 4-Salt strength observed to degrade in cyclic loading

Work Products



- 1- "Potential Effects of Compressed Air Energy Storage on Microbiology, Geochemistry, and Hydraulic Properties of Porous Aquifer Reservoirs", Kirk, Altman, and Bauer, SAND2010-4721
- "Potential Subsurface Environmental Impact of Compressed Air Energy Storage in Porous Bedrock Aquifers" Env. Sci. & Tech. (in Prep, Kirk et al)
- 2- "Considerations for Explosion Potential for CAES in a Depleted Natural Gas Reservoir", M. Grubelich
- 3- "Borehole and Formation Analyses in Reservoirs to Support CAES Development", S. Webb
- 4- "Experimental Deformation of Salt in Cyclic Loading", S. Bauer and S. Broome, Solution Mining Research Institute April 2010 SAND2010-1805

Statement about future tasks



- 1- Develop map for US regions with geology potentially suitable for CAES
- 2- Borehole parametric study
- 3-Continue evaluation of cyclic loading effects on salt and reservoir rocks







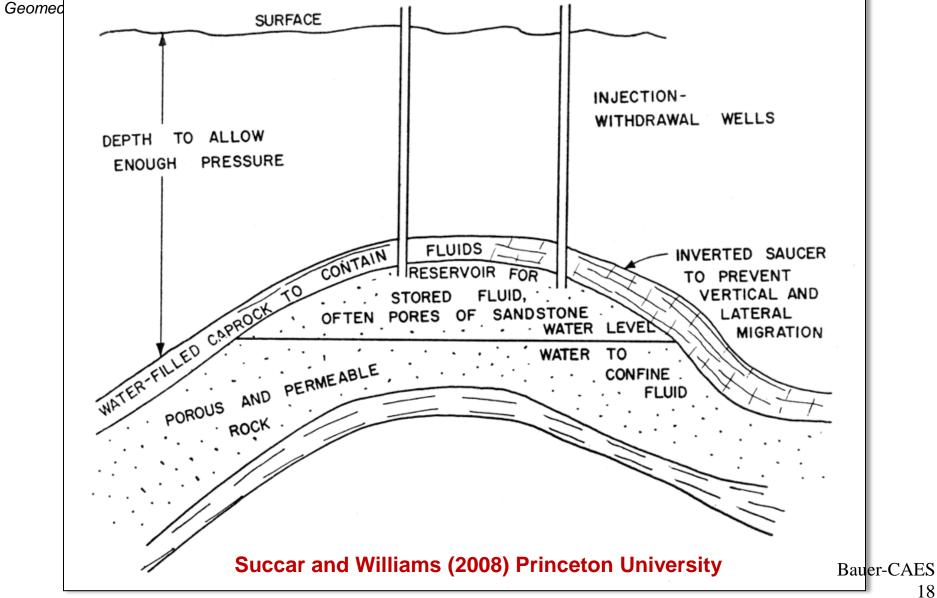
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Potential Microbial and Chemical Impact of CAES in a Sandstone

Matthew Kirk
Geochemistry Department

Compressed air energy storage

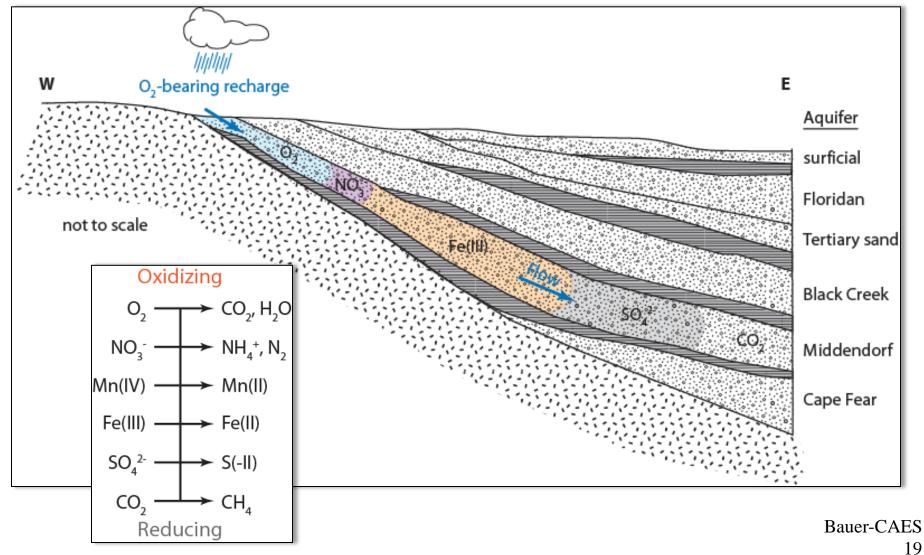




Groundwater microbiology

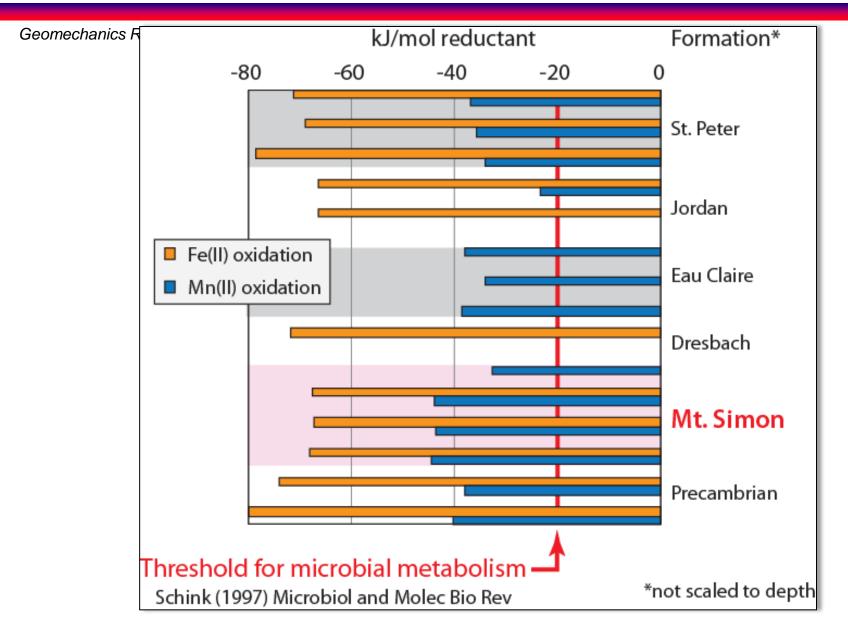


Example: Middendorf coastal plain aquifer, South Carolina



Metabolic energy available for Fe(II) and Mn(II) oxidation in the Mt. Simon

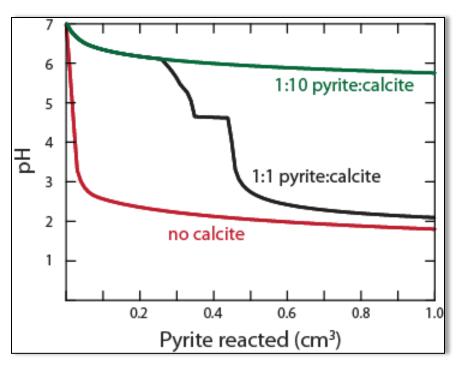


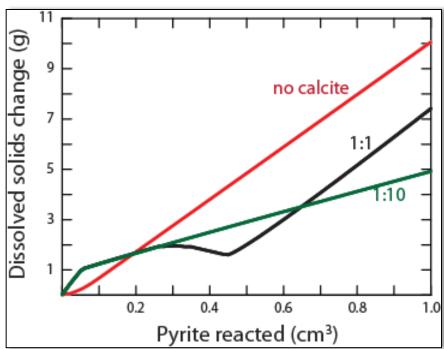


Effect of pyrite oxidation on groundwater composition



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Geochemist's Workbench reaction path model assuming 0.2 fO₂

• no calcite: pyrite + 3.75 O₂ + 3.5 H₂O \rightarrow Fe(OH)₃ + 2 SO₄²⁻ + 4 H⁺

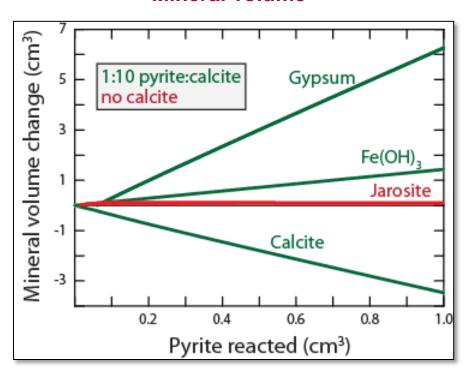
• with calcite: pyrite + 2 calcite + 3.75 O_2 + 1.5 $H_2O \rightarrow Fe(OH)_3$ + 2 SO_4^{2-} + 2 Ca^{2+} + 2 CO_2

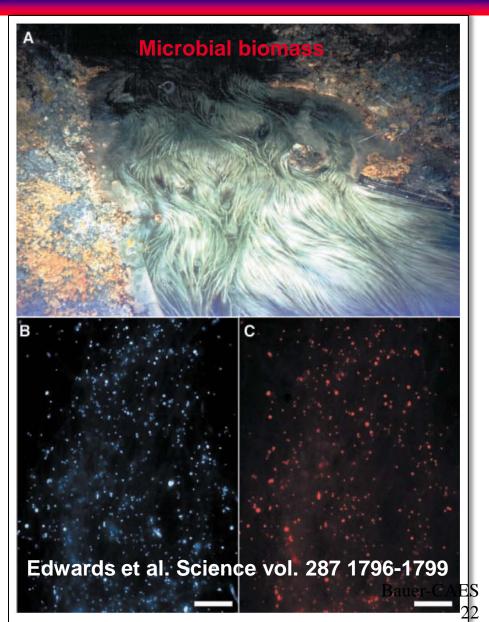
Effect of Pyrite Oxidation on Porosity



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Mineral volume





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Considerations for Explosion Potential for CAES in a Depleted Natural Gas Reservoir

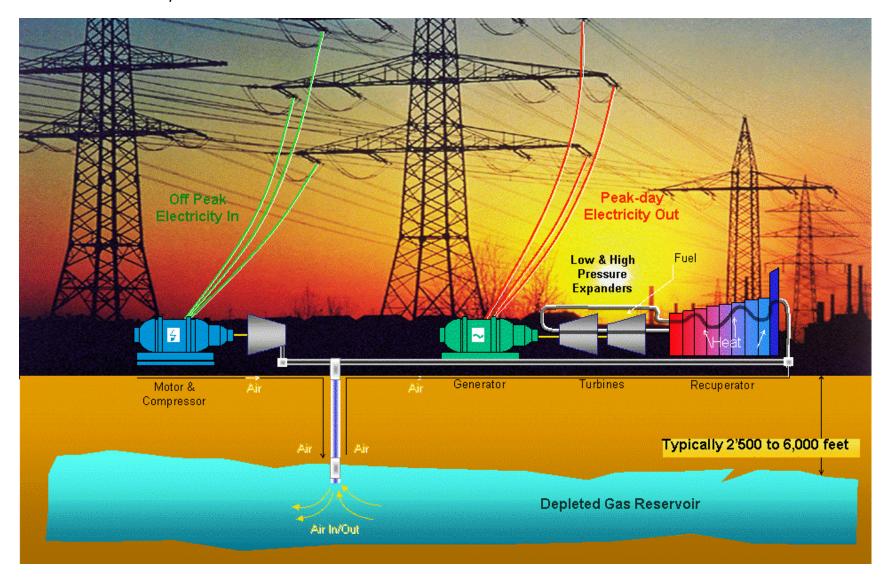


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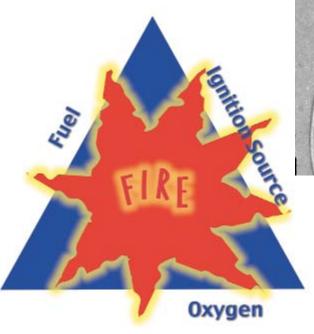
Compressed Air Energy Storage

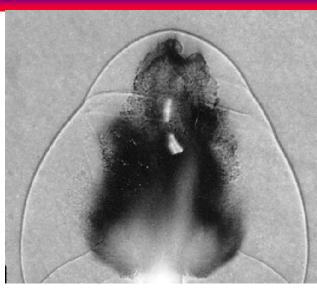


Fuel, Oxygen & Ignition Source









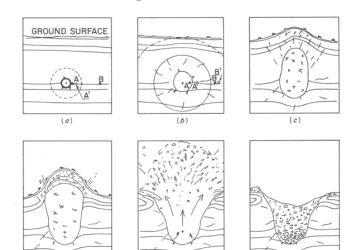
Detonation, reaction proceeds at supersonic speeds (shock wave).

Combustion or Deflagration 10's to 100's of ft/sec reaction rates.

Why worry?



- The pressure rise ratio for a confined deflagrating (unvented) fuel air mixture is ~9:1
- The peak pressure ratio for a detonating fuel air mixture is ~ 18:1
- Both events could be severe: (rough calculation in progress)





Important Points

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Depleted gas reservoir

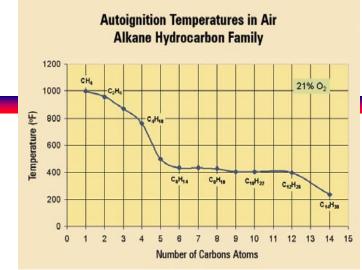
- What does depleted mean?
- At atmospheric pressure?
 - What is the residual natural gas composition?
 - Why is this important?
 - Heavy hydrocarbons change the ignition window and decrease the ignition temperature

Natural gas composition

Component	Typical Analysis (mole %)	Range (mole %)		
Methane	95.2	87.0 - 96.0		
Ethane	2.5	1.5 - 5.1		
Propane	0.2	0.1 - 1.5		
iso - Butane	0.03	0.01 - 0.3		
normal - Butane	0.03	0.01 - 0.3		
iso - Pentane	0.01	trace - 0.14		
normal - Pentane	0.01	trace - 0.04		
Hexanes plus	0.01	trace - 0.06		
Nitrogen	1.3	0.7 - 5.6		
Carbon Dioxide	0.7	0.1 - 1.0		
Oxygen	0.02	0.01 - 0.1		
Hydrogen	trace	trace - 0.02		

Table 6. — Limits of flammability of combustible vapors in air and oxygen at 25° C and 1 atm¹

tupoto in an ana oxygen at 20 o ana t ann						
	Flammability limits, vol pct					
Combustible	Air		Oxygen			
	L ₂₅	U ₂₅	L ₂₅	U ₂₅		
HYDROCARBONS						
Methane Ethane Propane n-Butane n-Hexane n-Heptane	5.0 3.0 2.1 1.8 1.2 1.1	15.0 12.4 9.5 8.4 7.4 6.7	5.0 3.0 2.3 1.8 1.2	61 66 55 49 ² 52 ² 47		
Acetylene Ethylene Propylene α-Butylene	2.5 2.7 2.4 1.6	100 36 11 10	≤2.5 2.9 2.1 1.8	100 80 53 58		
Cyclopropane	2.4 ² 1.3	10.4 ² 7.9	2.5 ≤1.3	60 N A		



Ignition Window



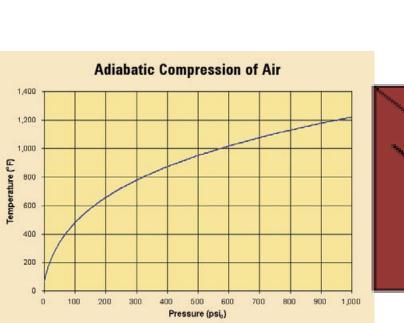
- Lower Flammability Limit (aka Lower Explosive Limit, LFL or LEL)
 - Below the LFL the mixture of fuel and air lacks sufficient <u>fuel</u> to react
 - Above the LFL deflagration or detonation possible
- Upper Flammability Limit (aka Upper Explosive Limit, UFL or UEL)
 - Above the UFL the mixture of fuel and air lacks sufficient <u>air</u> to react.
 - Below the UFL deflagration or detonation possible
- ~Ignition possible between 90 and 370 psi
 - Assuming well mixed conditions and starting at 1atmosphere NG
 - ~Below 90 psi too rich and above 370 psi too lean
 - Example: Flight 800 center tank explosion
 - Lean on the ground & rich at cruise altitude
 - Above the LFL and below the UFL during climb
 - Ignition source present
 - Boom!

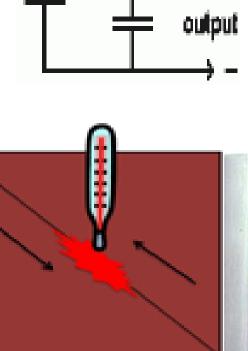


Ignition Sources 0.3 mJ=0.0002 ft-lb= "not much"



- Adiabatic compression
- Piezo-electric discharge
- Static discharge
- Lightning strike
- Frictional heating







Results & Conclusions: Mitigation & Safety



- Purge reservoir before use
- Low pressure air cycling below UFL to remove gas (~90 psi)
- In-situ gas monitor
- Never draw down air below the LFL (370 psi)
- Insure no surface breach if ignition occurs (sufficient overburden)
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Stephen W. Webb





Conclusions

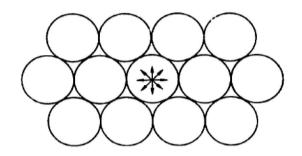


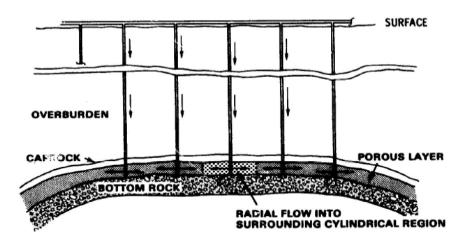
- Permeability Variation Much More Important then Porosity Variation
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Study geometry views



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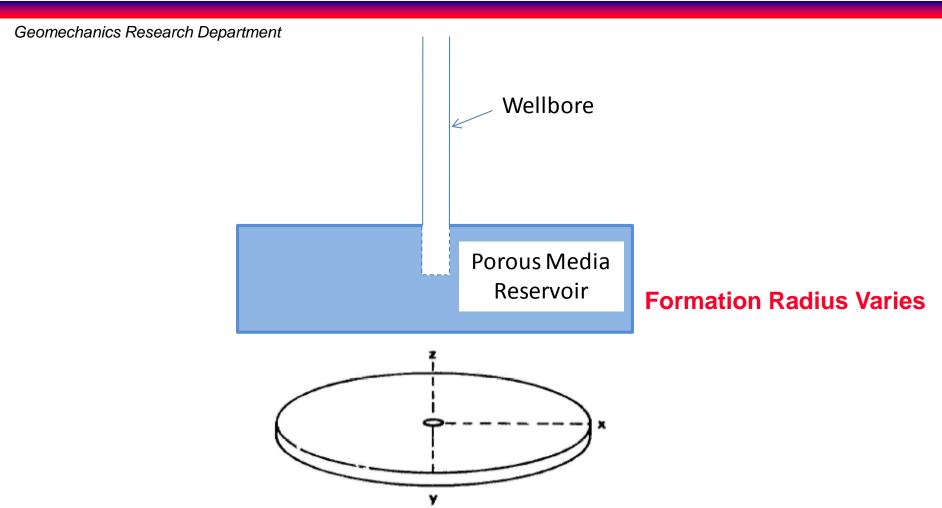




CAES Borehole Schematic (from Smith and Wiles, 1979)

CAES Borehole Study





Representative Borehole/Formation Geometry

Study Parameters



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Formation Height – 100 ft high

Depth – 2000 ft

Borehole Diameter – 7 inches

Partial Completion

Permeability – 100 mD to 2000 mD (500 mD Nominal)

Porosity – 0.1 to 0.3 (0.2 Nominal)

Formation Radius - Varies

Based on P_{max} and P_{min} Values

Mass Flows

See Cycle

Two-Phase Characteristic Curves

Leverett J-Function Scaling

Air Pressure Considerations



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P<sub>min</sub>
Turbine Inlet Pressure = 45 bar (4.5 MPa)
Pressure Drop to Surface = ~5 bar (0.5 MPa)
Minimum Borehole Pressure = 5.0 Bar
P<sub>max</sub>
0.6 x Lithostatic = 8.4 MPa
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Maximum Borehole Pressure = 8.4 MPa

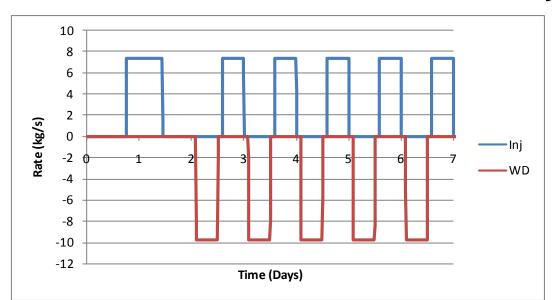
Pressure Cycling Model



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CAES Cycle

- Based on Smith and Liles (1979)
- 10% Mass Cycled Per Week
- 40% Air Added on the Weekend
- Mass Rates Based on Available Mass
 - » Function of Formation Radius, Porosity, Gas Saturation



Typical Cycle

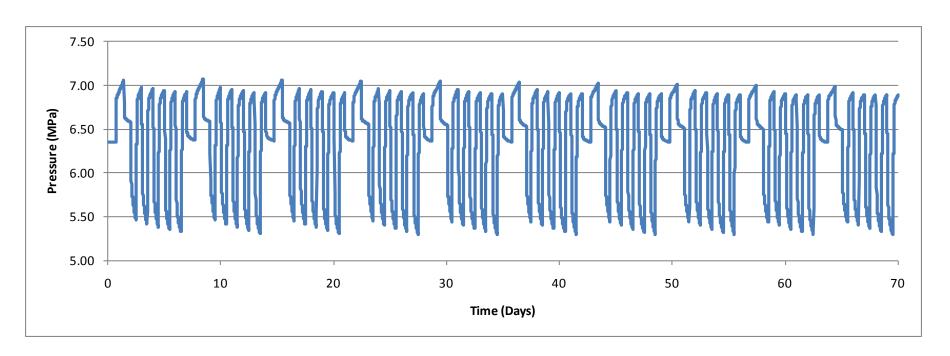
Borehole pressure



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Typical Cycle Results for Borehole Pressure

After Formation of Bubble



Procedure for Given Permeability and Porosity



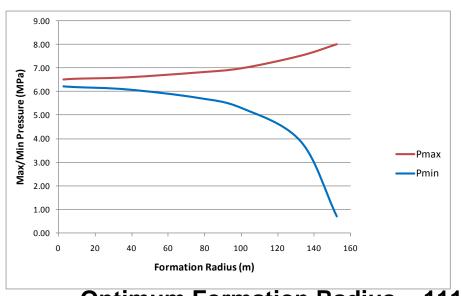
- Formation Radius Increase
 - Mass Rates Increase Larger Available Mass in Formation
 - P_{max} Increases
 - P_{min} Decreases
- Optimum Formation Radius and Mass Flow Rate When P_{max} and/or P_{min} Met

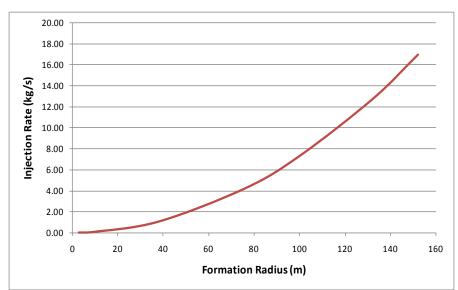
CAES Borehole Study



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Typical Results (k = 500 mD, ϕ = 0.2)

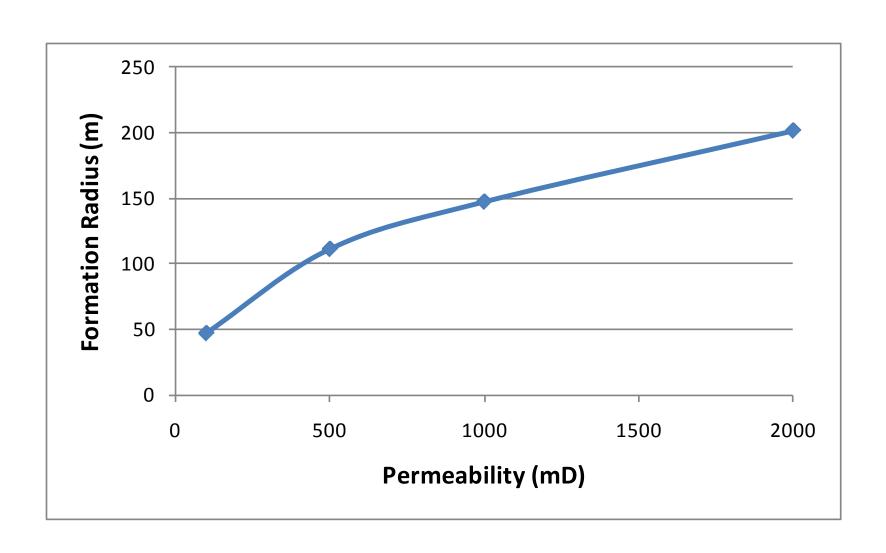




Optimum Formation Radius = 111 m Based on P_{min}

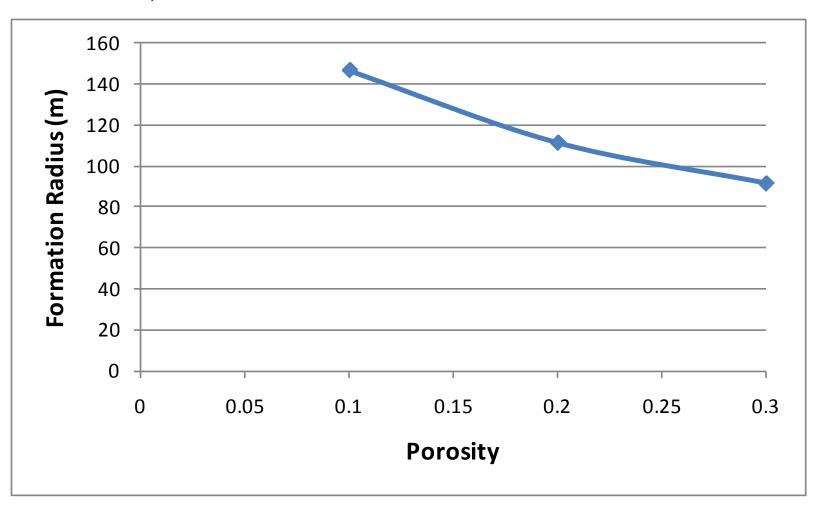
Permeability Variation





Porosity Variation





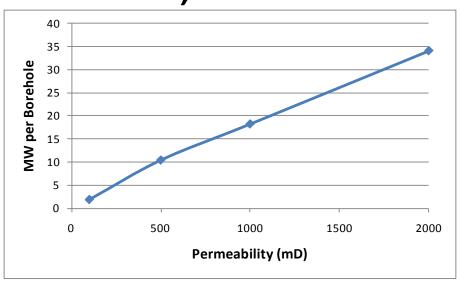
Permeability/Porosity vs. Power

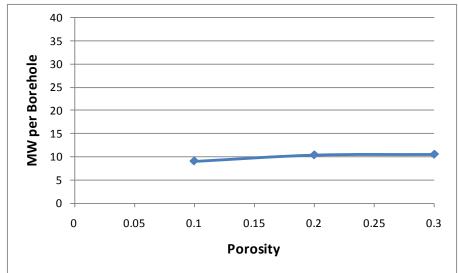


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Using Typical Turbine Parameters

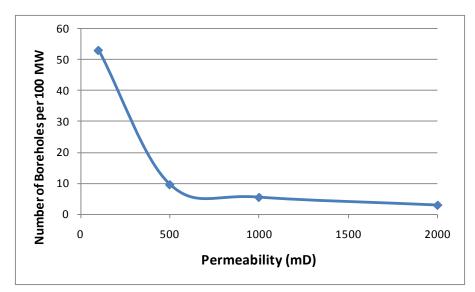
Based on Iowa CAES Power Density (~5 MW/m³) Scaled by Formation Pressure (Succar, 2008)

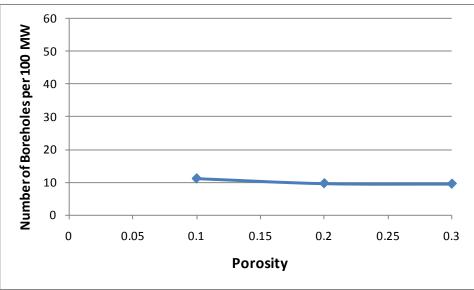




Number of Boreholes vs Permeability & Porosity







Conclusions



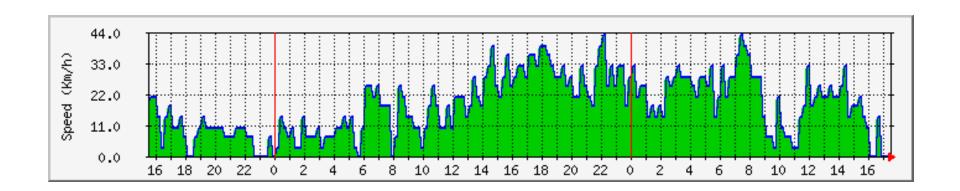
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Material Degradation (T-M-C-H effects) Due to Cyclic Loading



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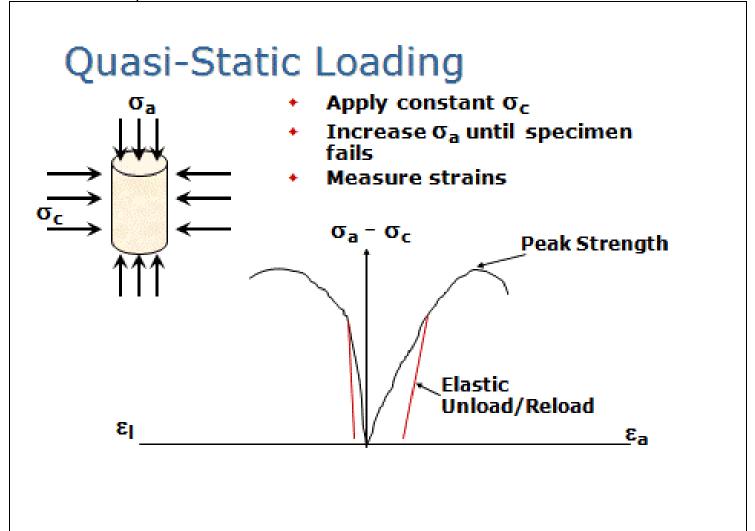
Experimental Deformation of Salt in Cyclic Loading SJ Bauer and ST Broome



Hourly fluctuations in wind speed could translate to frequent pressurization/depressurizations of salt caverns

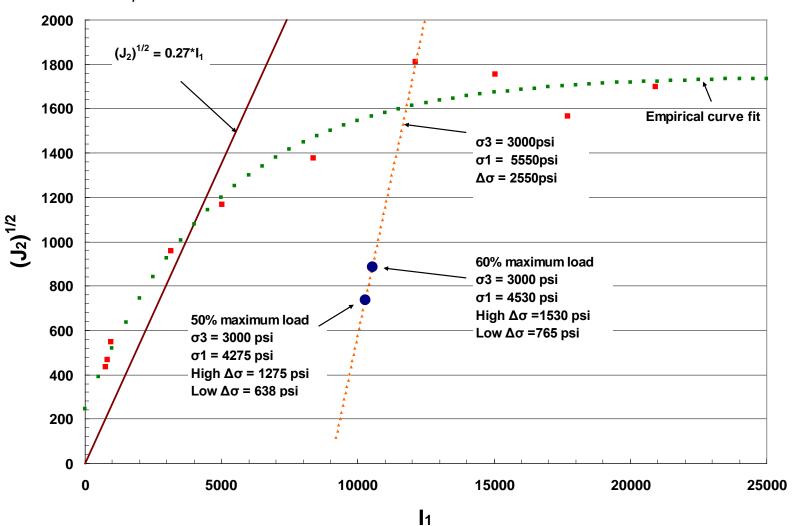
Experimental Deformation of Salt in Cyclic Loading





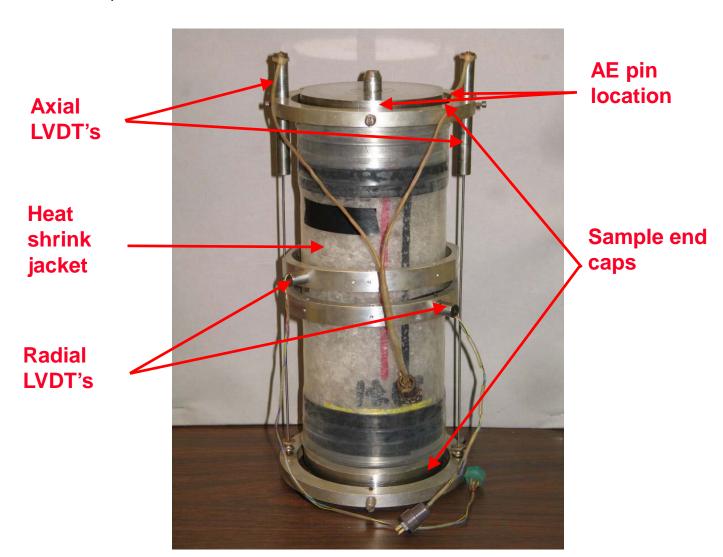
Dilatant behavior of salt determined from quasi-static tests and stress states for this study





Test assembly

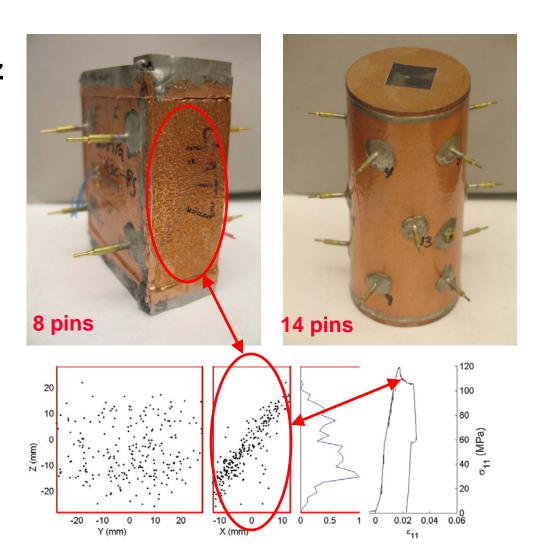




Acoustic Emissions System

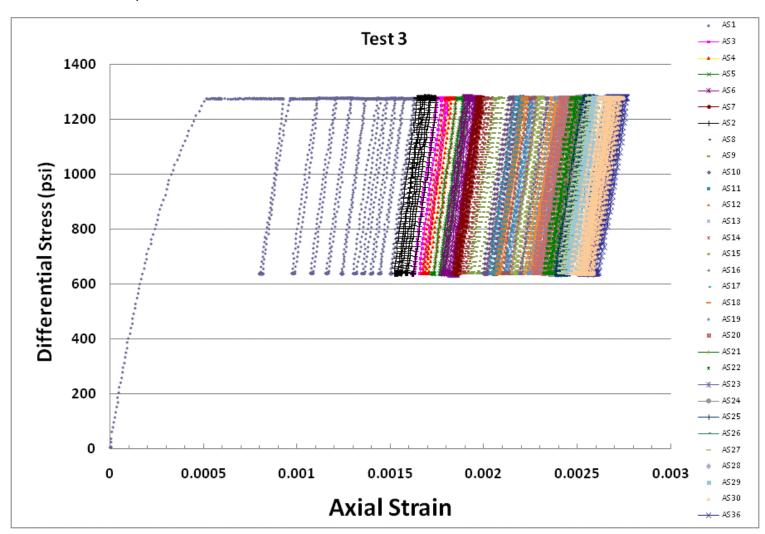


- Sample rates up to 25 MHz
- Typically acquire 3000 samples/event
- Tailor a discriminator to only sample events of a given criteria
- 60 dB amplifier
- Location of events is possible with many pins









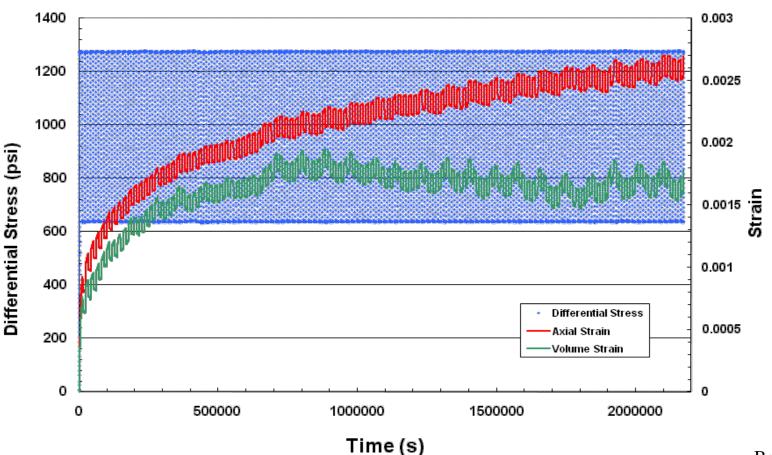
Test data



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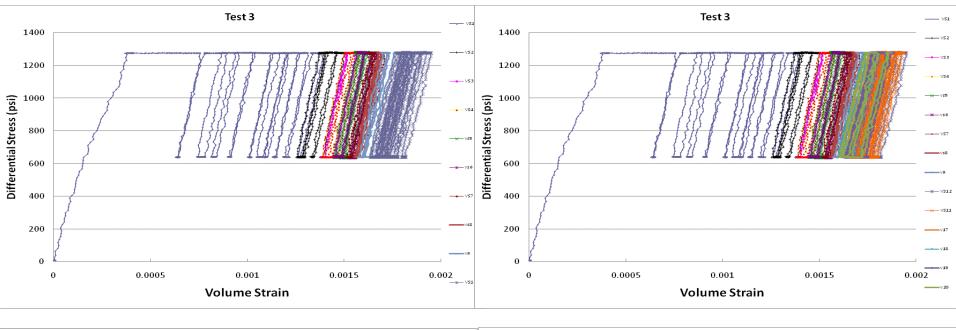
Differential stress, axial and volume strain versus time, Test 3.

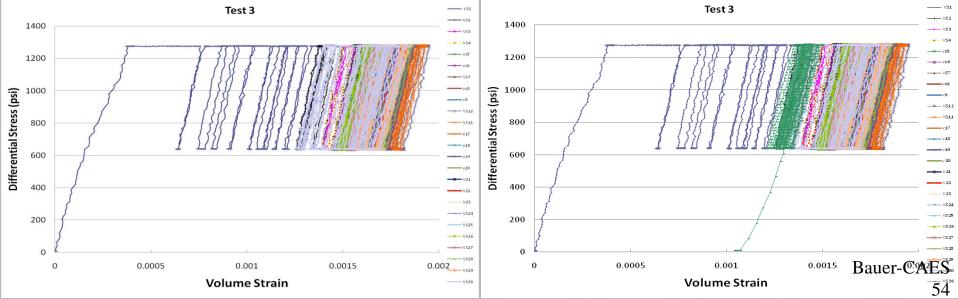
Test3

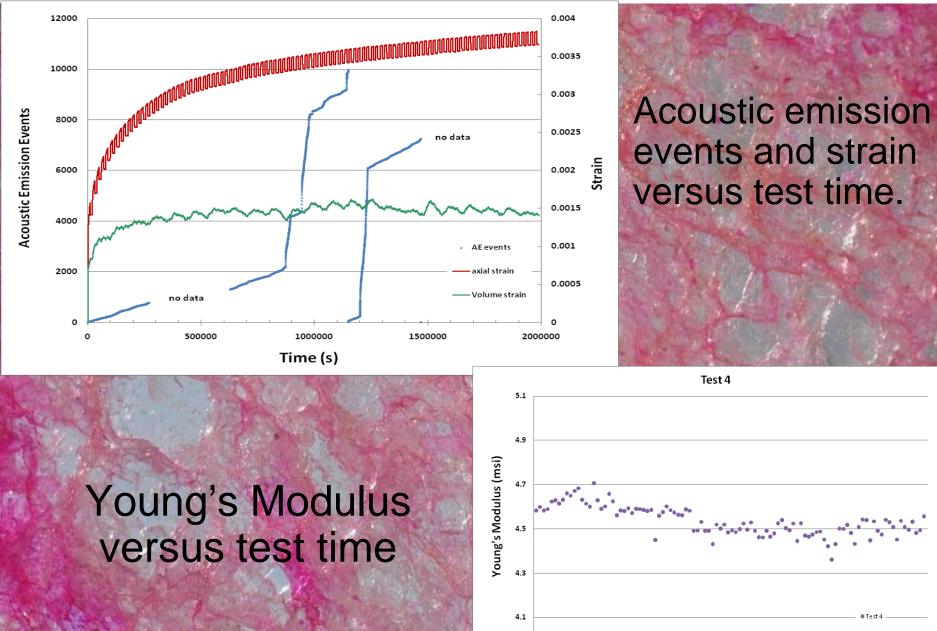


Differential stress versus volume strain, Test 3









55

Bauer-CAES

Time (s)

Concluding Comments



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