

# **MODULAR CONNECTION TECHNOLOGIES FOR SC WALLS OF SMRS**

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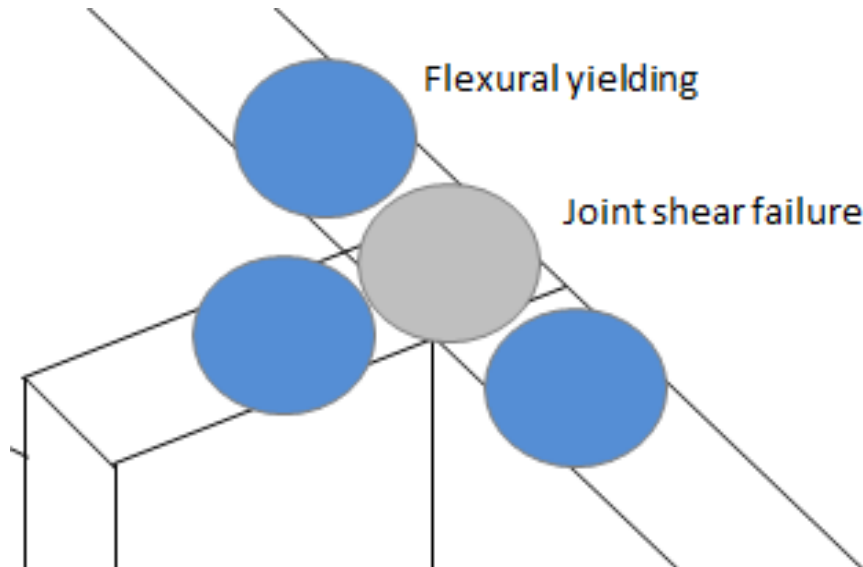
# OUTLINE

- SC Wall-to-Wall T Connection
- SC Wall-to-Wall L Connection
- Benchmarking Analysis
- SC Slab-to-Wall Connection
- Findings

# SC WALL-TO-WALLT CONNECTION

## *DESIGN PHILOSOPHY*

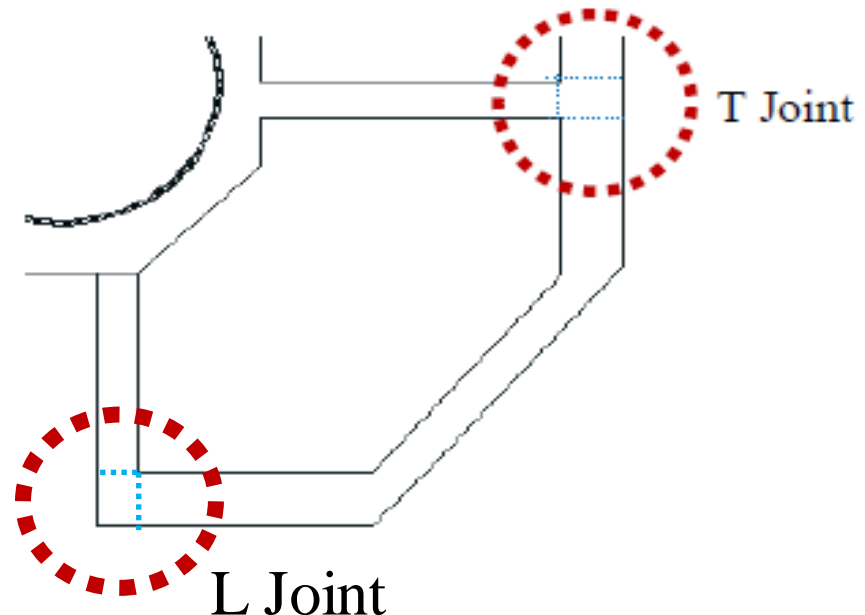
- Full-strength connection design philosophy
  - Develops the expected strength
- Implementation of full-strength design
  - Two parts in SC wall joints
    - SC wall and SC wall joints
  - Desired failure mode
    - Flexural yielding (ductile) – plastic hinges



# SC WALL-TO-WALL CONNECTION DESIGN PHILOSOPHY

- SC wall-to-wall joints in the CIS
  - Common joint configurations (T and L)
- Implementation of full-strength design
  - The required joint shear strength
    - Based on the force transfer mechanism
  - Calculation of the available joint shear strength
    - ACI 349-06 equation
    - $\gamma = 12$  for SC wall T-joints
    - $\gamma = 8$  for SC wall L-joints
    - Verification is required

$$V_n = \gamma \sqrt{f'_c} A_j$$



# SC WALL-TO-WALLT CONNECTION

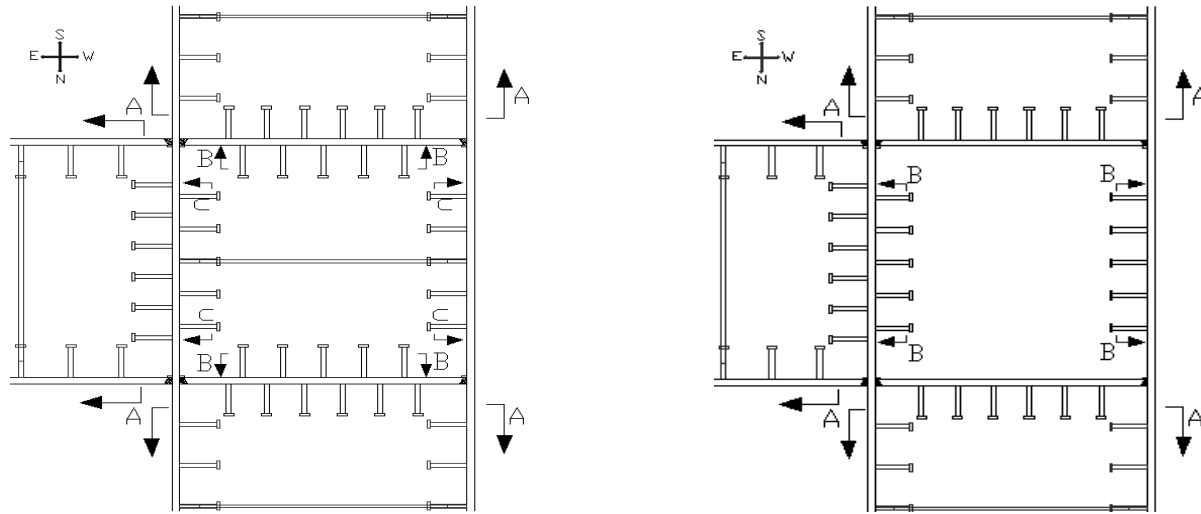
## *Experimental Program*

- Four full-scale SC wall T-joint shear specimens
  - T = 30 in.
  - To evaluate the influence of (i) the shear reinforcement ratio and (ii) The steel headed stud layout
  - Designed to undergo joint shear failure

Specimen	Steel faceplate thickness, $t_p$ (in.)	Steel tie plate dimension		No. of tie plates in the Joint	Shear Stud Layout
		Continuous SC wall	Discontinuous SC wall		
JS-T1-F	0.75	$3\frac{3}{4} \times \frac{5}{16}$ in.	$3\frac{3}{4} \times \frac{1}{2}$ in.	1	F
JS-T0-F	0.75	$3\frac{3}{4} \times \frac{5}{16}$ in.	$3\frac{3}{4} \times \frac{1}{2}$ in.	0	F
JS-T0-P	0.75	$3\frac{3}{4} \times \frac{5}{16}$ in.	$3\frac{3}{4} \times \frac{1}{2}$ in.	0	P
JS-T2-F	0.75	$3\frac{3}{4} \times \frac{5}{16}$ in.	$3\frac{3}{4} \times \frac{1}{2}$ in.	2	F

# SC WALL-TO-WALL CONNECTION

## *Experimental Program*



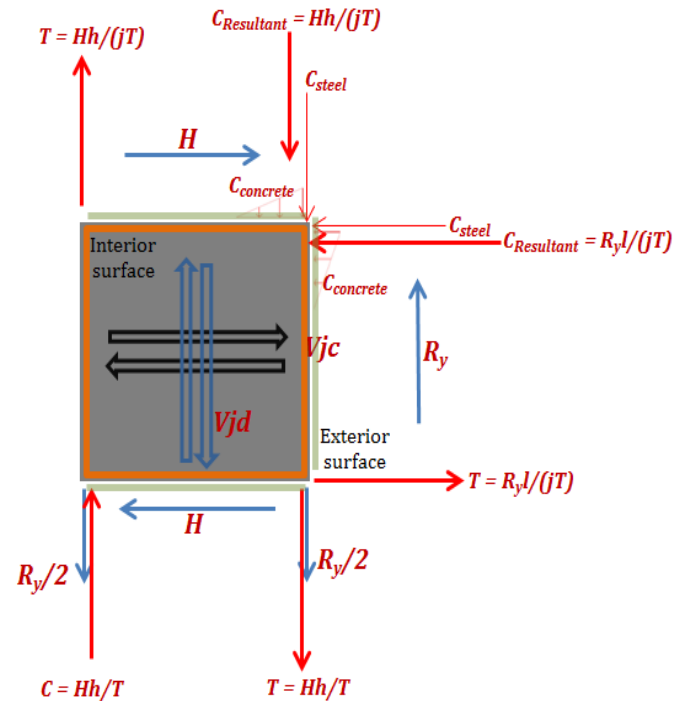
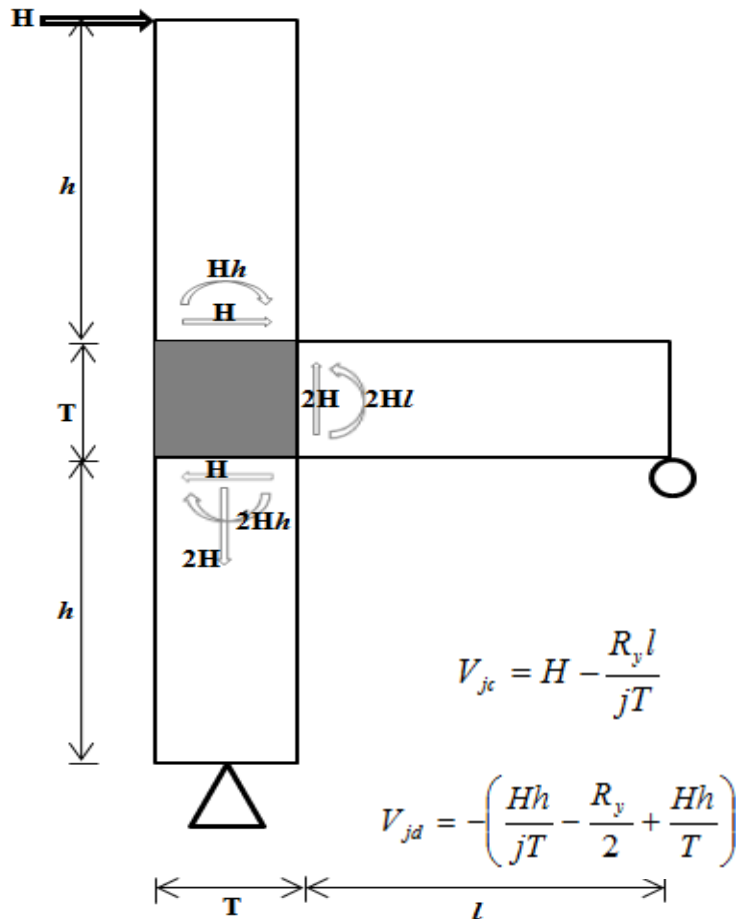
### ○ Material properties

Specimen	Faceplates		Tie plates		Studs	Concrete, psi
	$F_y$ , ksi	$F_u$ , ksi	$F_y$ , ksi	$F_u$ , ksi	$F_u$ , ksi	
JS-T1-F	58.6	83.9	60.4	69.1	74.0	6,473
JS-T0-F	58.0	77.0	62.7	73.5	80.9	6,402
JS-T0-P	58.0	77.0	62.7	73.5	80.9	6,502
JS-T2-F	58.5	78.6	62.7	73.5	80.9	6,504
						Avg = 6,502

# SC WALL-TO-WALLT CONNECTION

## Experimental Program

- Boundary conditions and joint shear force terms



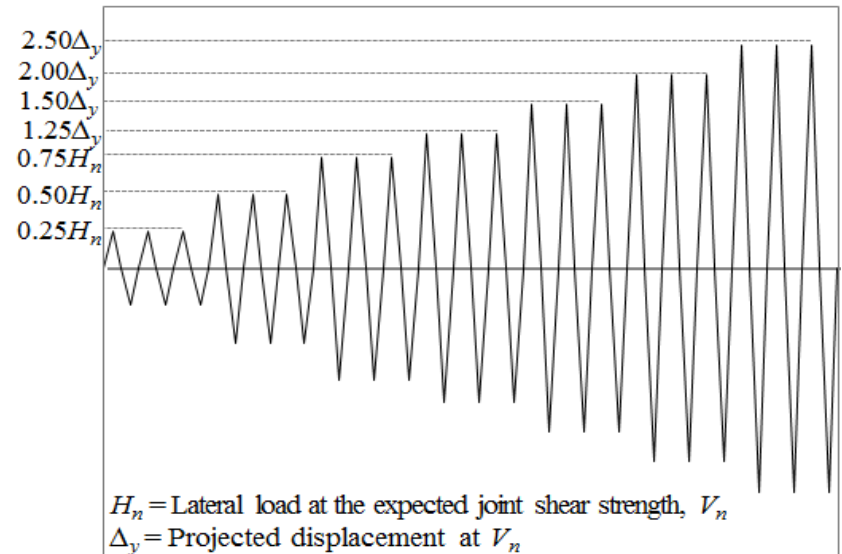
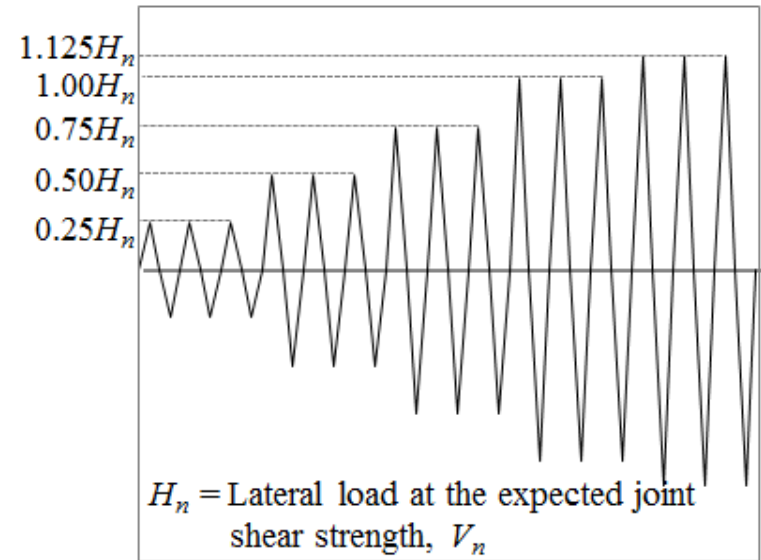
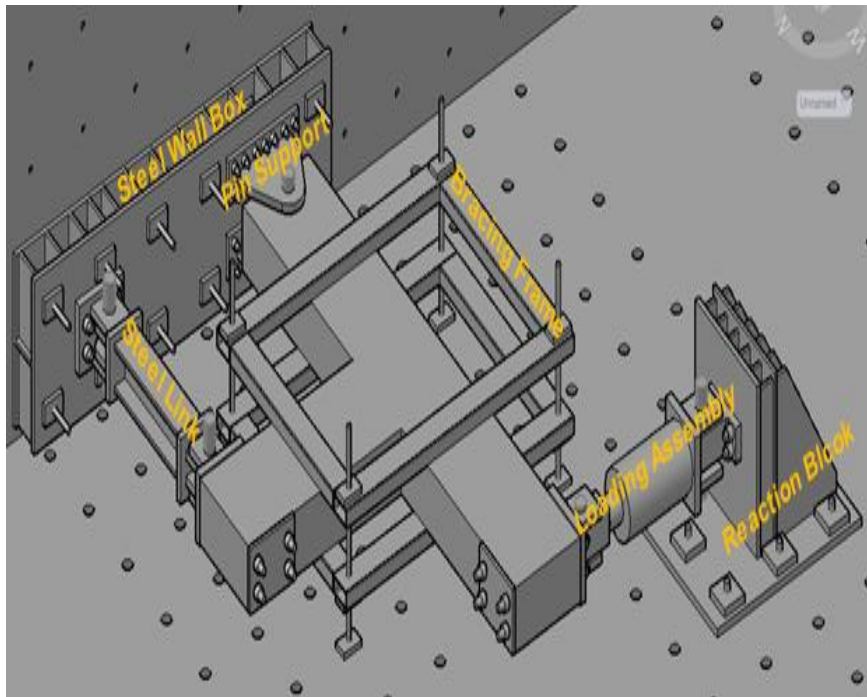
$$V_{jc} = H - \frac{R_y l}{jT}$$

$$V_{jd} = -\left(\frac{Hh}{jT} - \frac{R_y}{2} + \frac{Hh}{T}\right)$$

# SC WALL-TO-WALLT CONNECTION

## *Experimental Program*

- Test-setup and loading protocol





# SC WALL-TO-WALLT CONNECTION

## *Experimental Program*

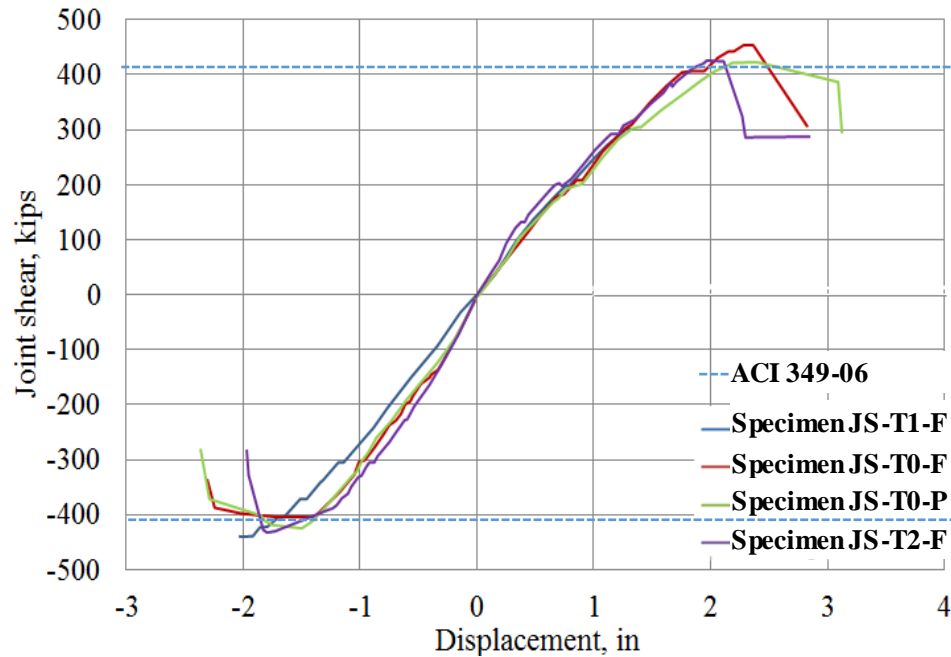
### ○ Summary of experimental results

Specimen	Ultimate joint shear, kips	Shear strain at the ultimate joint shear	Governing failure mode	Event order in the Joint region
JS-T1-F	438.4	0.0049	Joint shear	Concrete crack ↓ Yielding of steel tie plate ↓ Extensive concrete cracking
JS-T0-F	455.5	0.0070	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T0-P	427.8	0.0069	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T2-F	431.6	0.0060	Joint shear	Concrete crack ↓ Yielding of steel tie plates ↓ Extensive concrete cracking

# SC WALL-TO-WALLT CONNECTION

## *Experimental Program*

### ○ Joint shear – displacement response



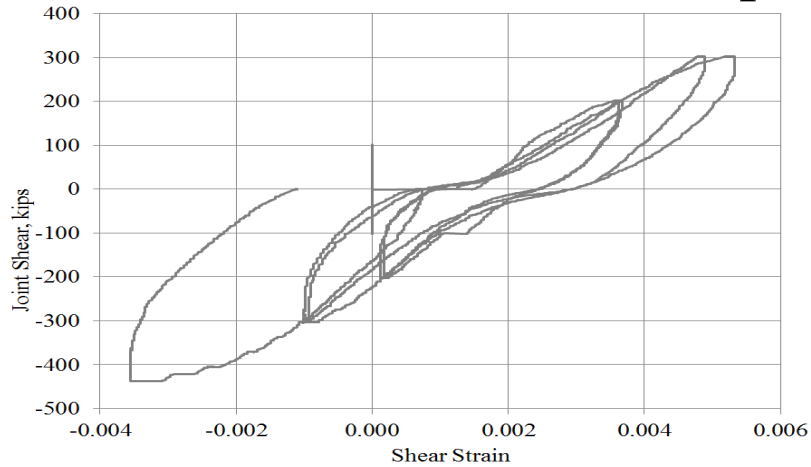
$$V_{js} - \Delta'$$

- $V_{njs}^{TEST}$  within the range of 426.7 - 454 kips
- Greater than  $V_{njs}^{ACI-exp}$  (413 kips) by 3.1 - 10.3%.

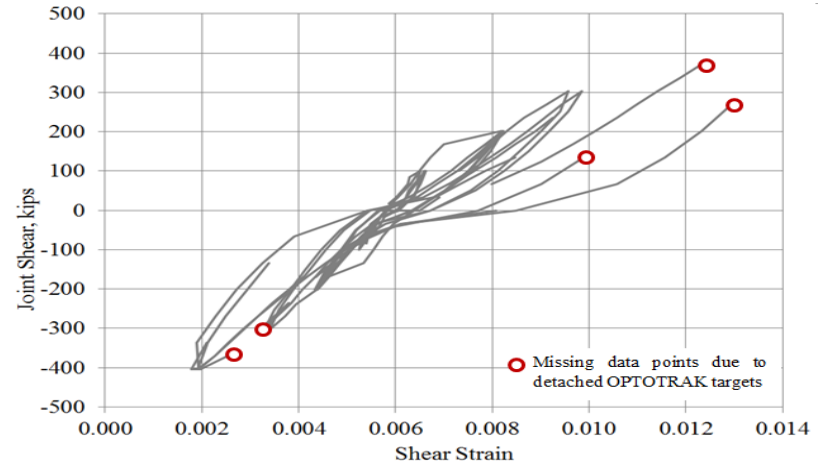
# SC WALL-TO-WALLT CONNECTION

## *Experimental Program*

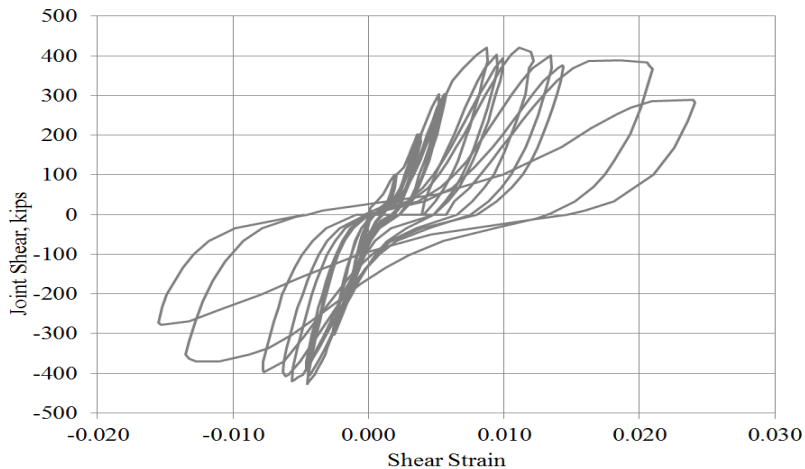
### ○ Joint shear – shear strain response



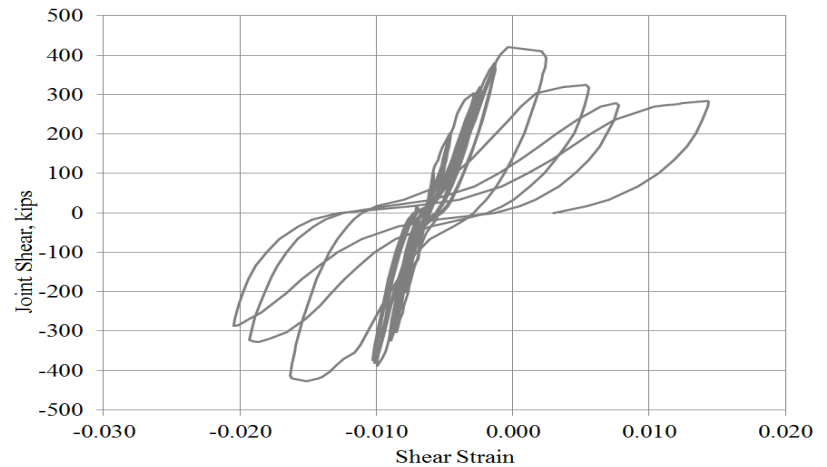
JS-T1-F



JS-T0-F



JS-T0-P

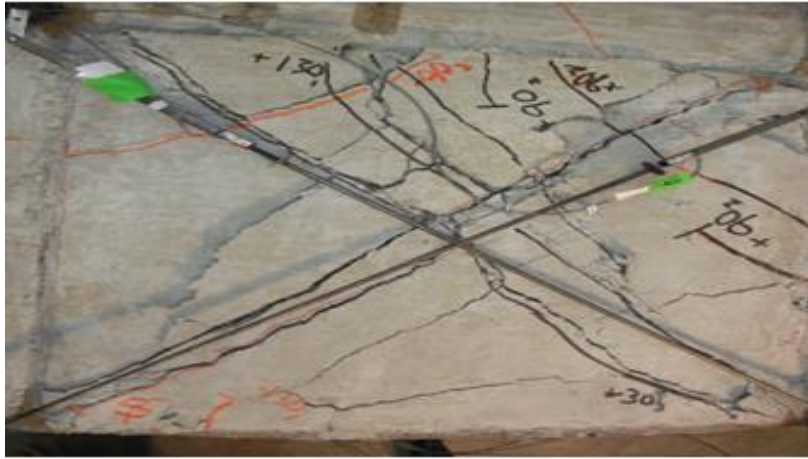


JS-T2-F

# SC WALL-TO-WALLT CONNECTION

## *Experimental Program*

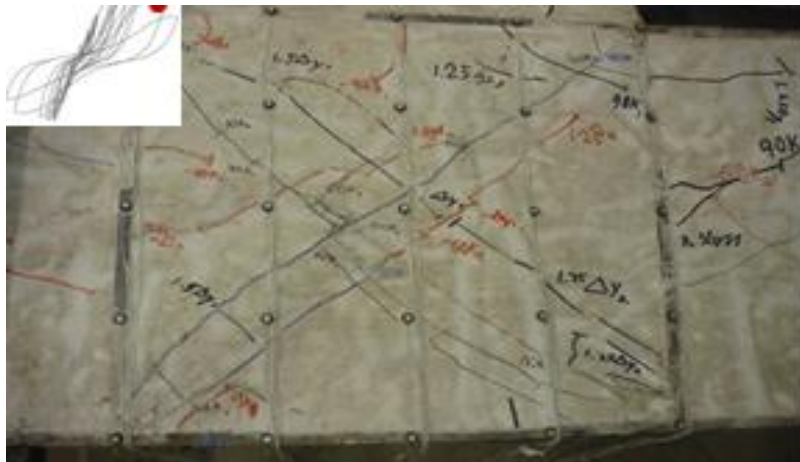
- Crack pattern at the ultimate joint shear : all specimens



JS-T1-F



JS-T0-F



JS-T0-P



JS-T2-F

# SC WALL-TO-WALL CONNECTION

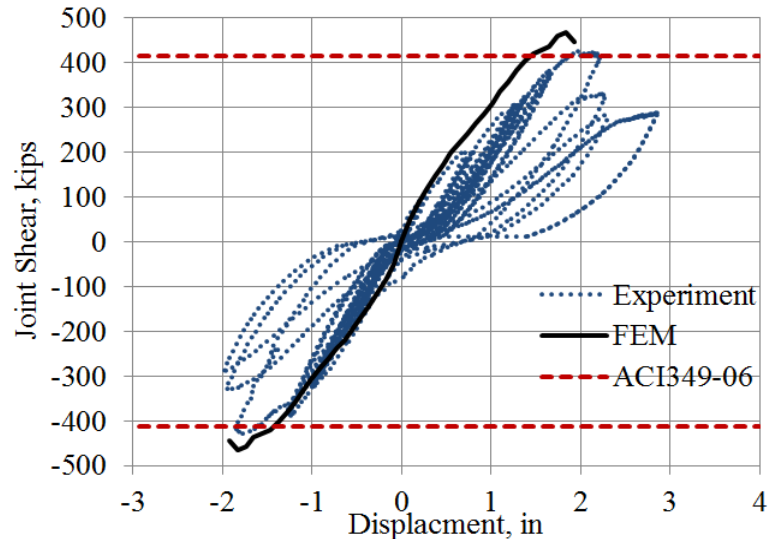
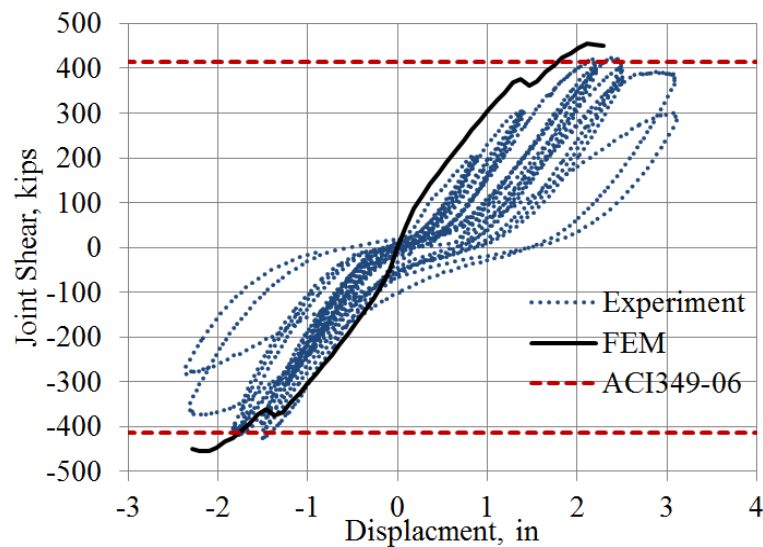
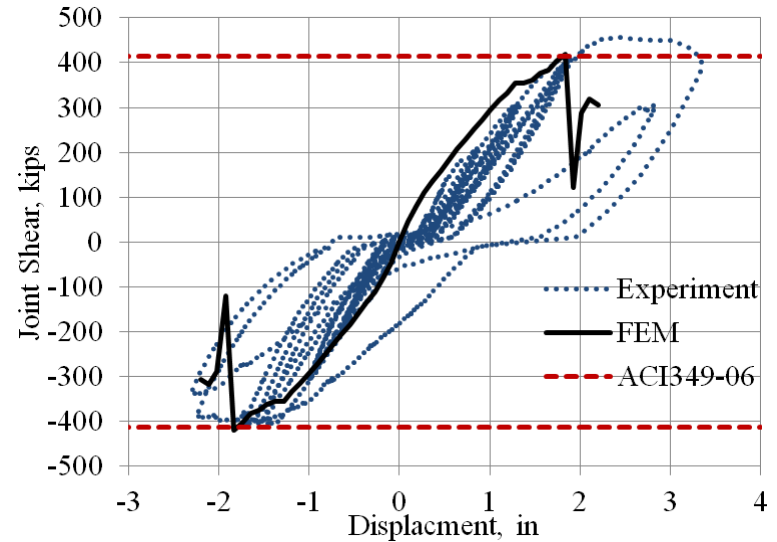
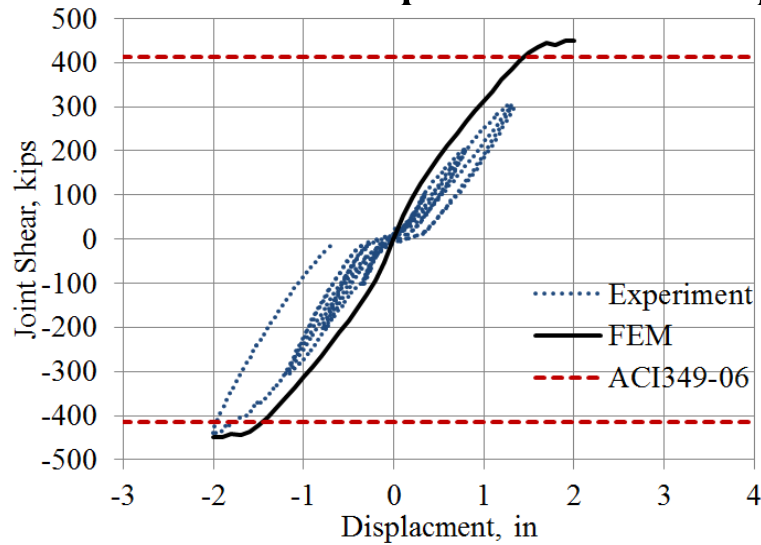
## *Benchmarking Analysis*

- 3-D FE analysis for additional insights
- Comparison with experimental results
- ABAQUS explicit
  - The quasi static analysis
  - Shell (S4R) elements for steel, solid (C3D8R) elements for concrete, and Timoshenko beam elements (B32) for stud
  - Connector elements (CONN3D2)
- CEF concrete model
  - Elastic in compression, Uniaxial tension strength and post-peak behavior defined in CEB-FIP mc 90 (1993)
  - Element deletion to prevent excessive deformation
- Steel material model
  - Multi-axial plasticity theory
  - Idealized uniaxial stress-strain curve

# SC WALL-TO-WALL CONNECTION

## *Analysis Results*

### ○ Joint shear – displacement response



# SC WALL-TO-WALLT CONNECTION

## *Benchmarking Analysis*

### ○ Summary

Specimen	Ultimate joint shear, kips	Shear strain at the ultimate joint shear	Governing failure mode	Event Order in the Joint region
JS-T1-F	450.0	0.0157	Joint shear	Concrete crack ↓ Yielding of steel tie plate ↓ Extensive concrete cracking
JS-T0-F	418	0.0142	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T0-P	455.4	0.0164	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T2-F	465.6	0.0147	Joint shear	Concrete crack ↓ Yielding of steel tie plates ↓ Extensive concrete cracking

# SC WALL-TO-WALL CONNECTION

## *Experimental Program*

- One full-scale SC wall L-joint shear specimens
  - $T = 30$  in.
  - To experimentally investigate the joint shear behavior of SC wall-to-wall L joint
  - The same specimen design approach and test procedure from SC wall-to-wall T joint specimens

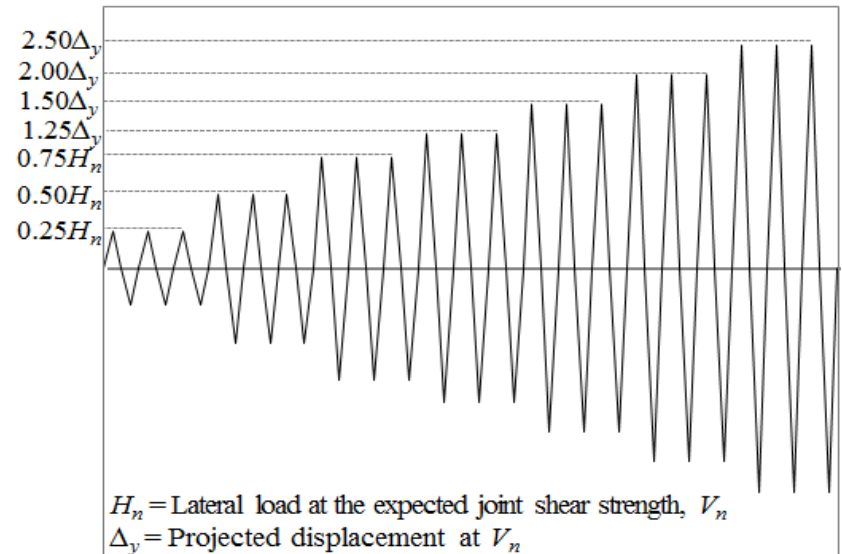
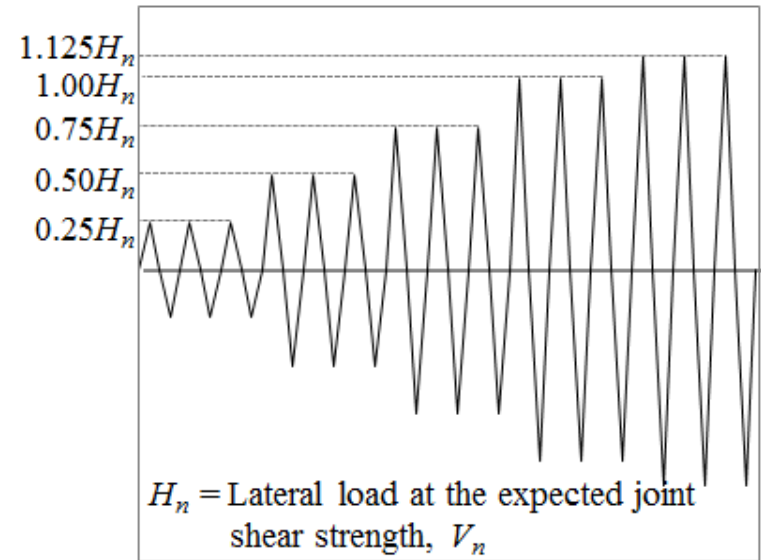
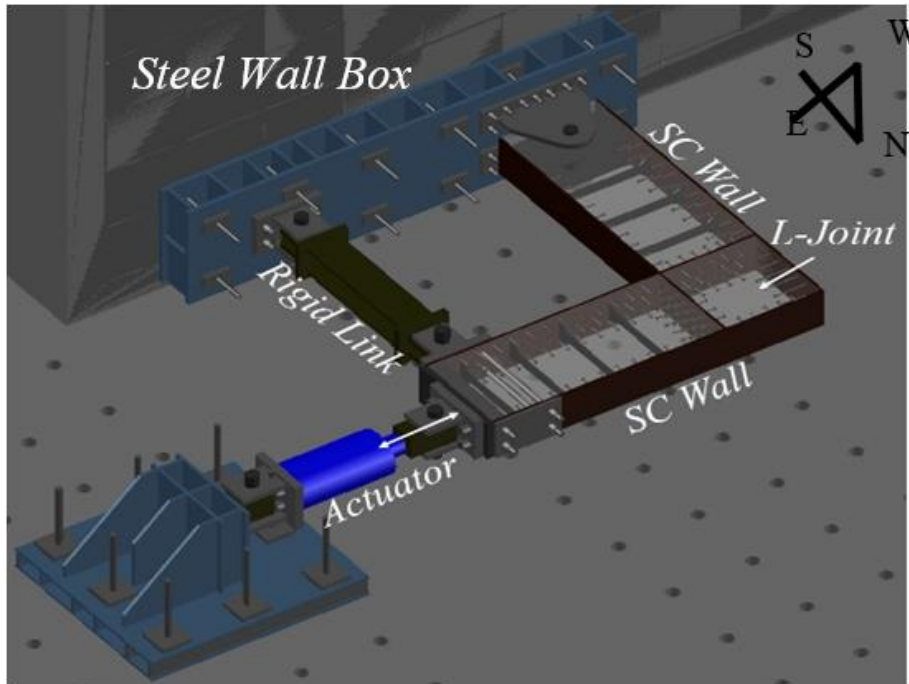
Specimen	Steel faceplate thickness, $t_p$ (in.)	Steel tie plate dimension		No. of tie plates in the Joint	Shear Stud Layout
		Continuous SC wall	Discontinuous SC wall		
JS-L-T0-F	0.75	$3\frac{3}{4} \times \frac{5}{16}$ in.	$3\frac{3}{4} \times \frac{1}{2}$ in.	0	F



# SC WALL-TO-WALL CONNECTION

## *Experimental Program*

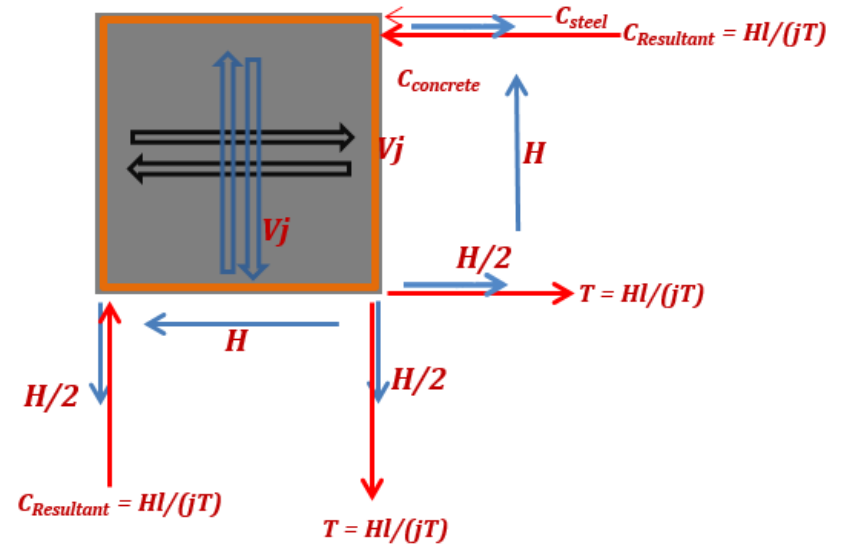
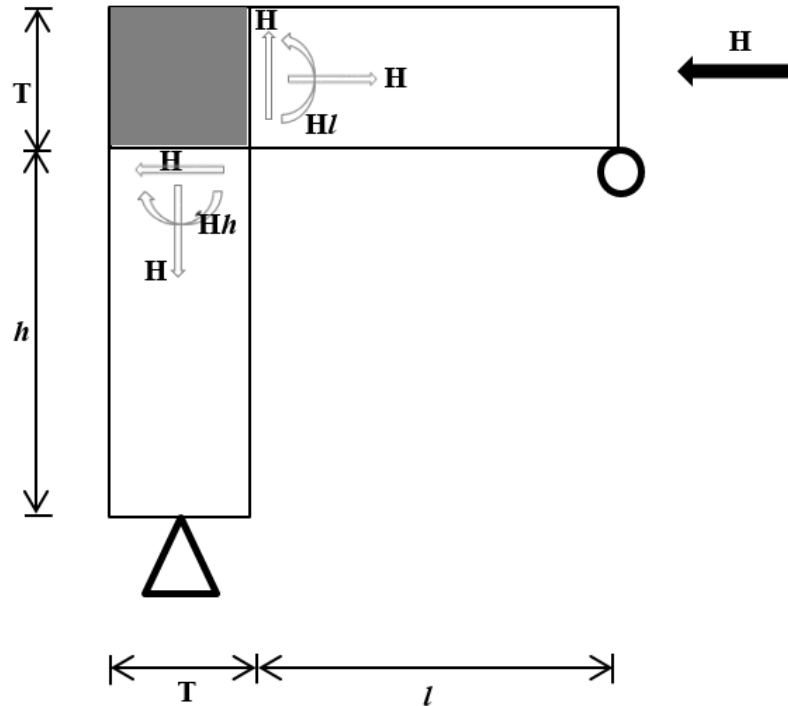
- Test-setup and loading protocol



# SC WALL-TO-WALLL CONNECTION

## *Experimental Program*

- Boundary conditions and joint shear force terms

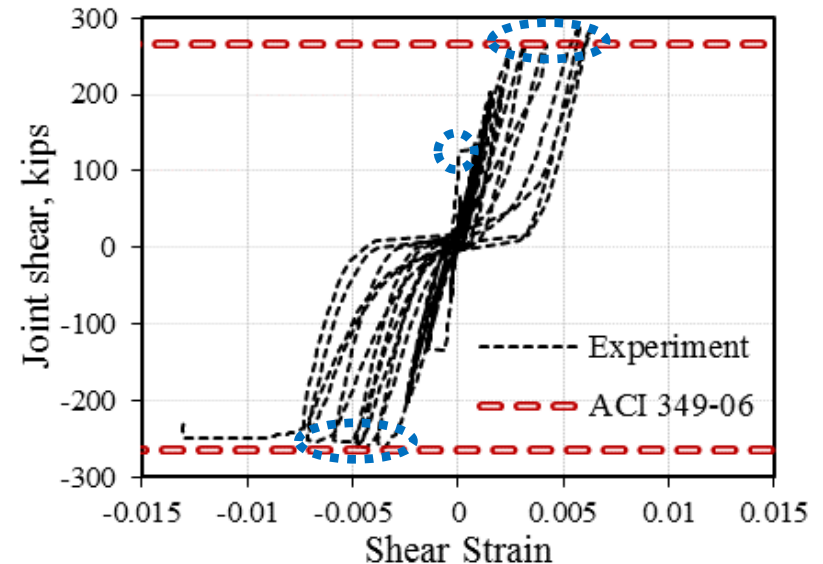
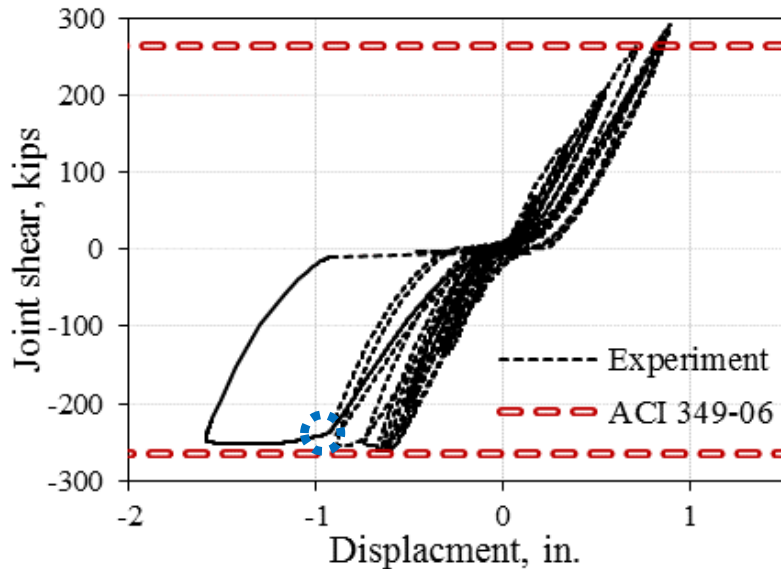


$$V_j = H \left( \frac{1}{2} - \frac{l}{jT} \right)$$

# SC WALL-TO-WALL CONNECTION

## *Experimental Program*

- Joint shear – displacement response



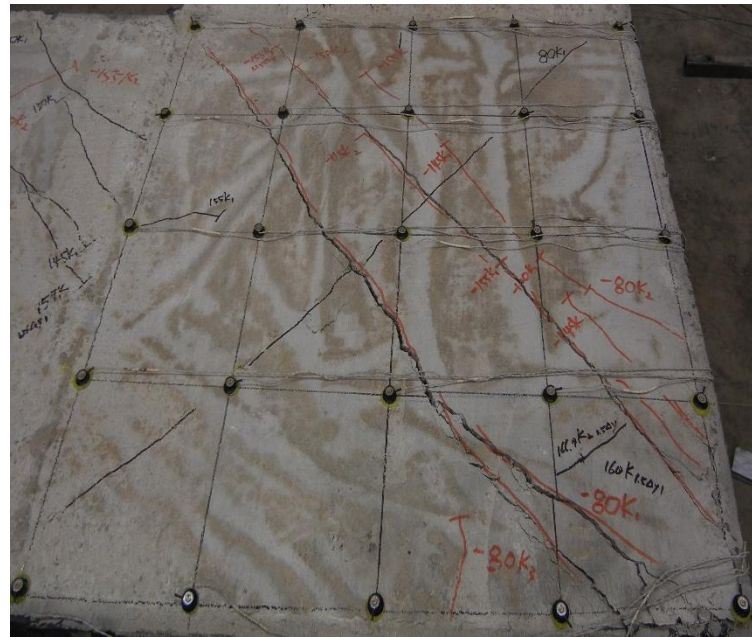
Ultimate joint shear, kips	Shear strain at the ultimate joint shear	Governing failure mode	Event order in the Joint region
261.7 (-) 290.3 (+)	- 0.0071 (-) 0.0089 (+)	Joint Shear Failure	Concrete crack ↓ Extensive concrete cracking ↓ Yielding of diaphragm plates

$$V_{njs}^{TEST} = 276 \text{ kips} \quad V_{njs}^{ACI-exp} (262.7 \text{ kips})$$

# SC WALL-TO-WALL CONNECTION

## *Experimental Program*

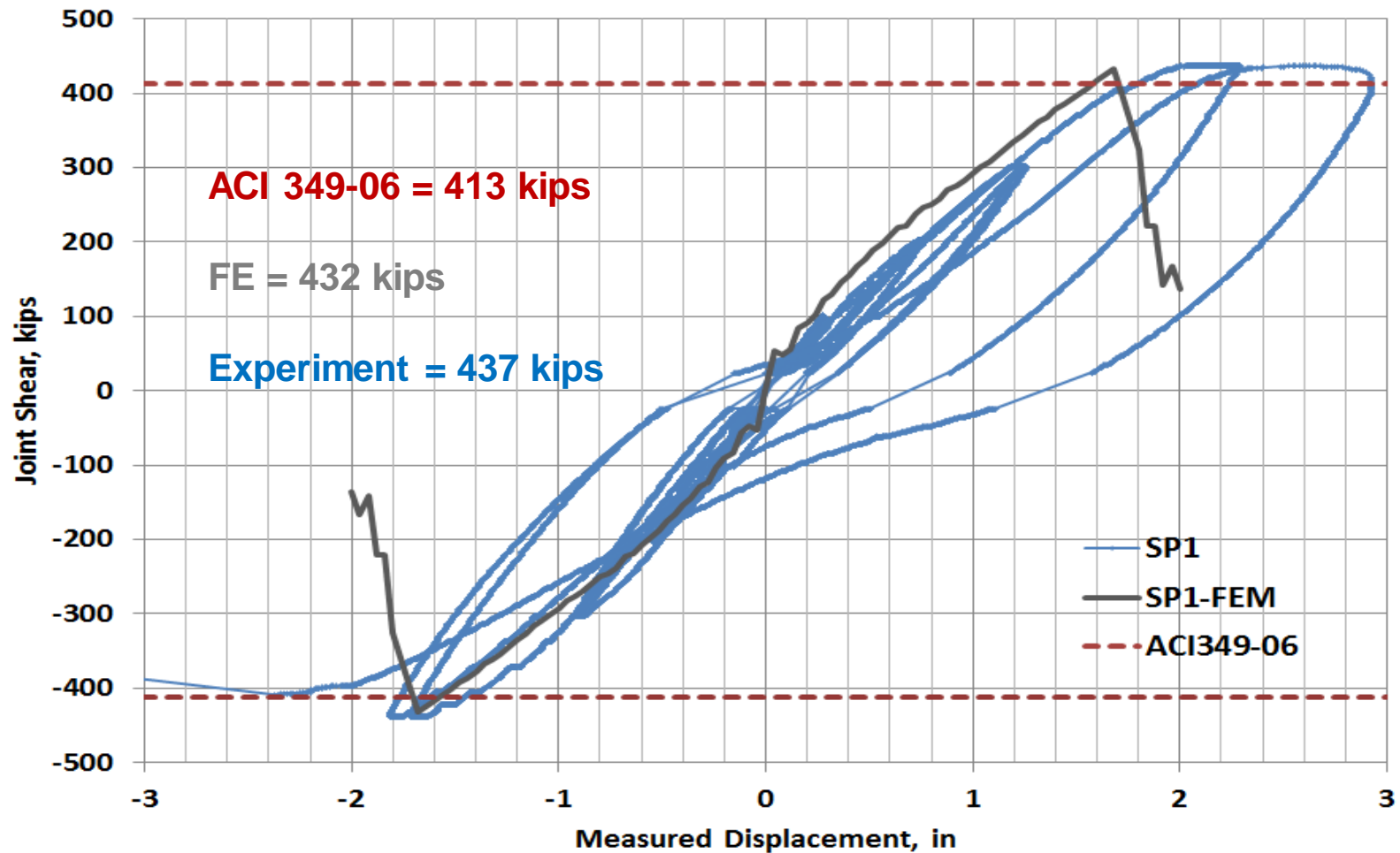
- Crack pattern at the ultimate joint shear



JS-L-T0-F

# BENCHMARKING ANALYSIS

- Analysis results – Specimen JS-T1-F
  - Joint shear – displacement response



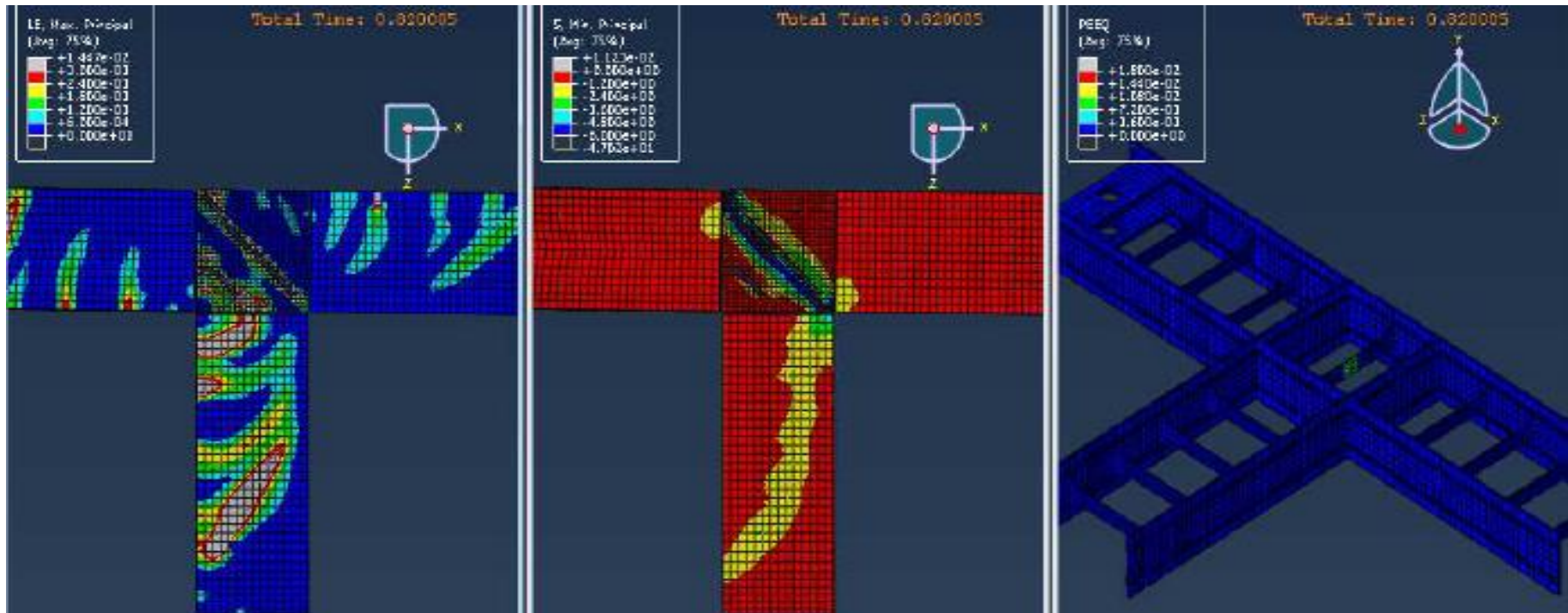
# BENCHMARKING ANALYSIS

- Analysis results – Specimen JS-T1-F
  - Stress and strain distribution

LE max

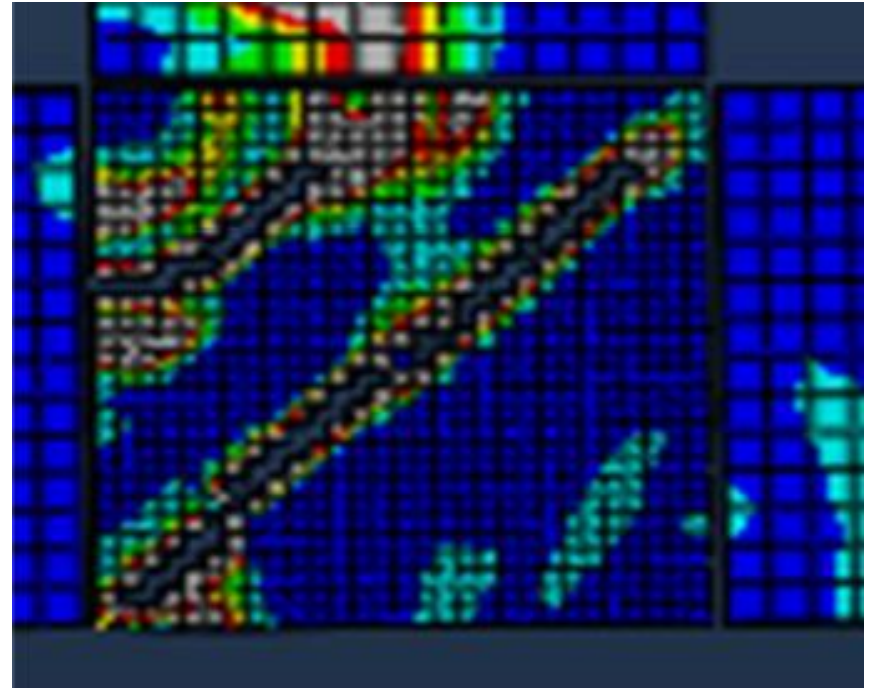
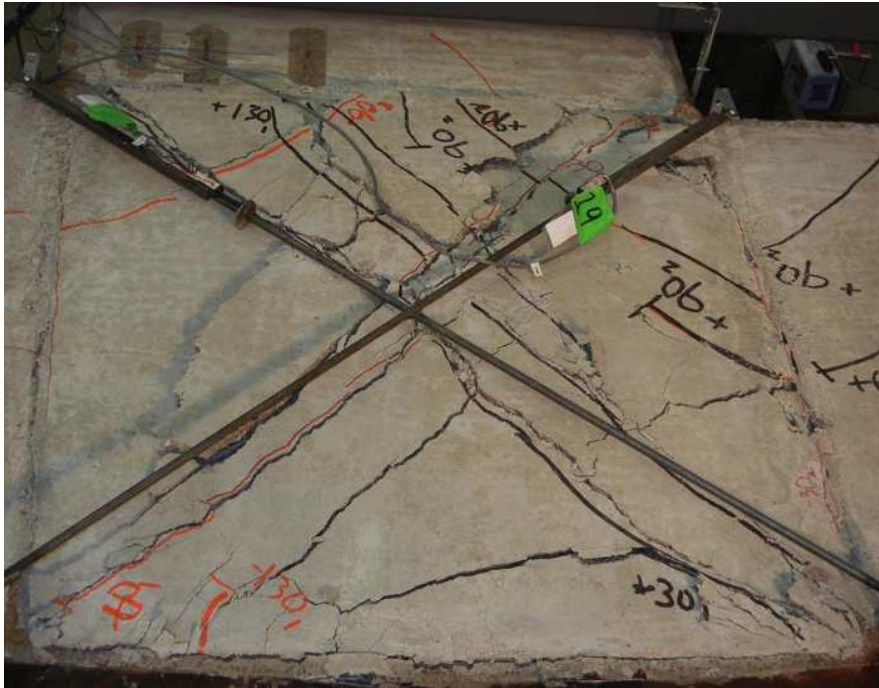
S min

PEEQ



# BENCHMARKING ANALYSIS

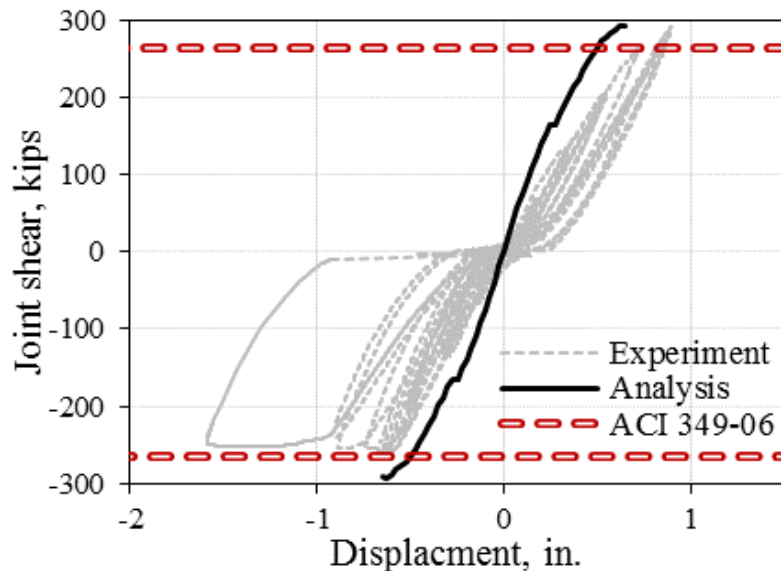
- Analysis results – Specimen JS-T1-F
  - Crack pattern



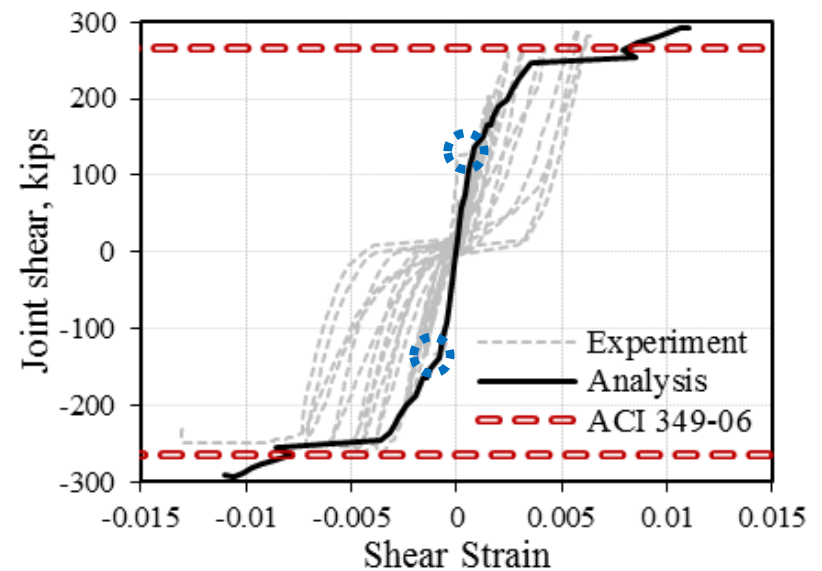
# BENCHMARKING ANALYSIS

- Analysis results – Specimen JS-L-T0-F

Joint shear – displacement response



Joint shear – shear strain response



- $V_{js}^{ACI349-06} = 262.7$  Kips (1.17MN)
- $V_{js}^{FEM} = 292.3$  Kips (1.3 MN) (+ 29.6 kips)
- $V_{js}^{Exp} = 276$  Kips (1.22 MN) (+ 13.3 kips)
- Joint shear failure

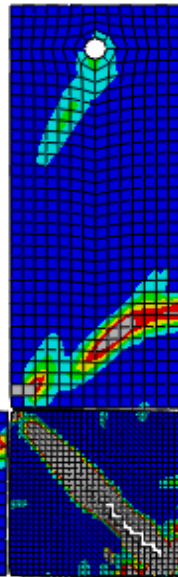
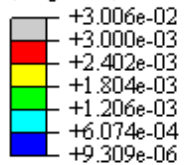


# BENCHMARKING ANALYSIS

- Analysis results – Specimen JS-L-T0-F
  - Stress and strain distribution

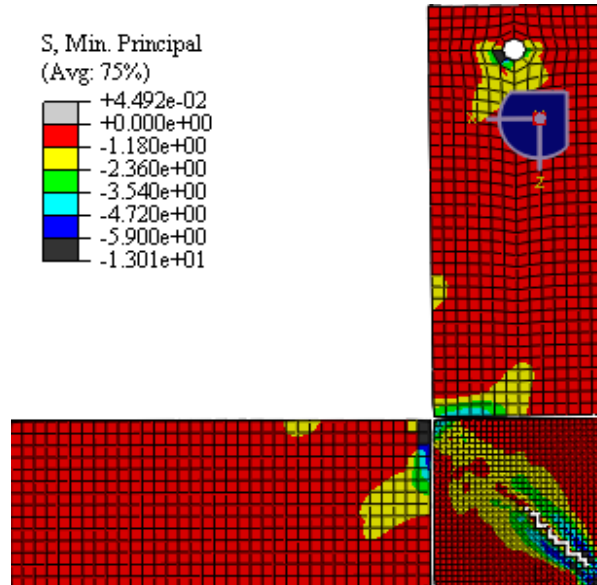
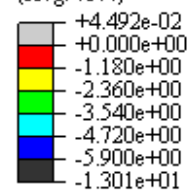
LE max

LE, Max. Principal  
(Avg: 75%)



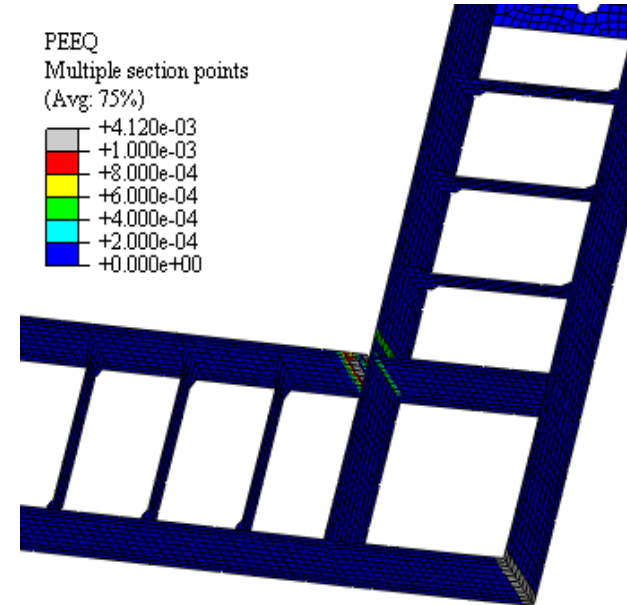
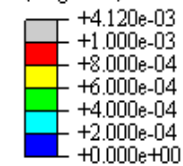
S min

S, Min. Principal  
(Avg: 75%)



PEEQ

PEEQ  
Multiple section points  
(Avg: 75%)



# SC SLAB-TO-WALL CONNECTION

## *Experimental Program*

### ○ Background

- Existing design recommendations and aids for RC slab (column) to slab connections
- No existing design recommendation for SC slab-to-wall connection
- The applicability of existing code provisions for RC slab (column) to slab connection on SC slab-to-wall connection

### ○ Design philosophy

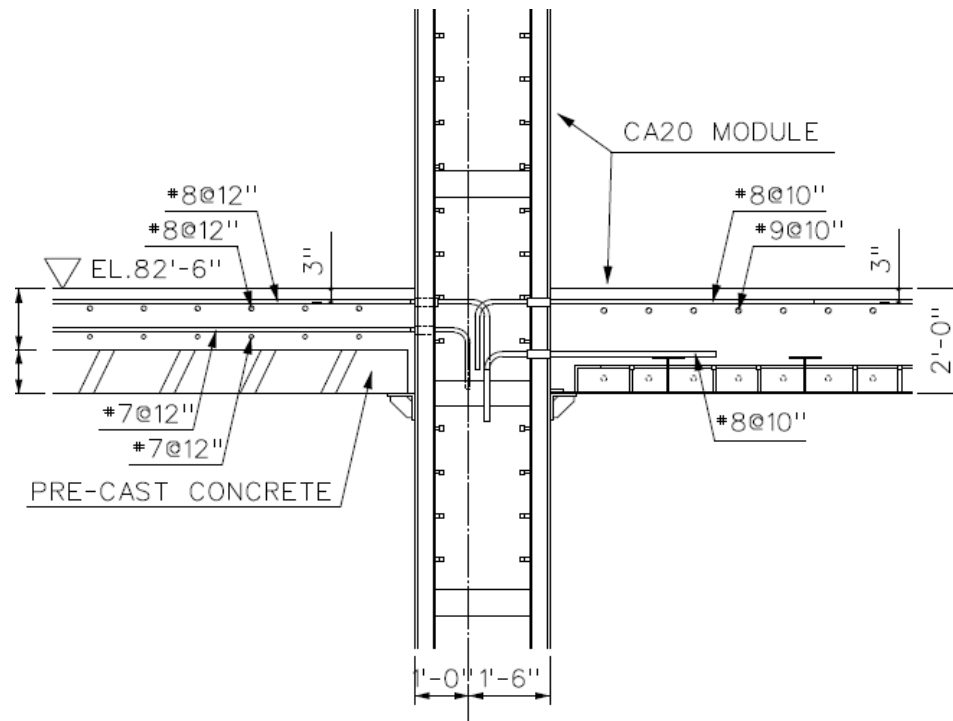
- The full strength connection design philosophy
- The connection region should not be the weakest point
- Capability of transferring both shear and flexural demand

# SC SLAB-TO-WALL CONNECTION

## *Experimental Program*

### ○ Test parameters

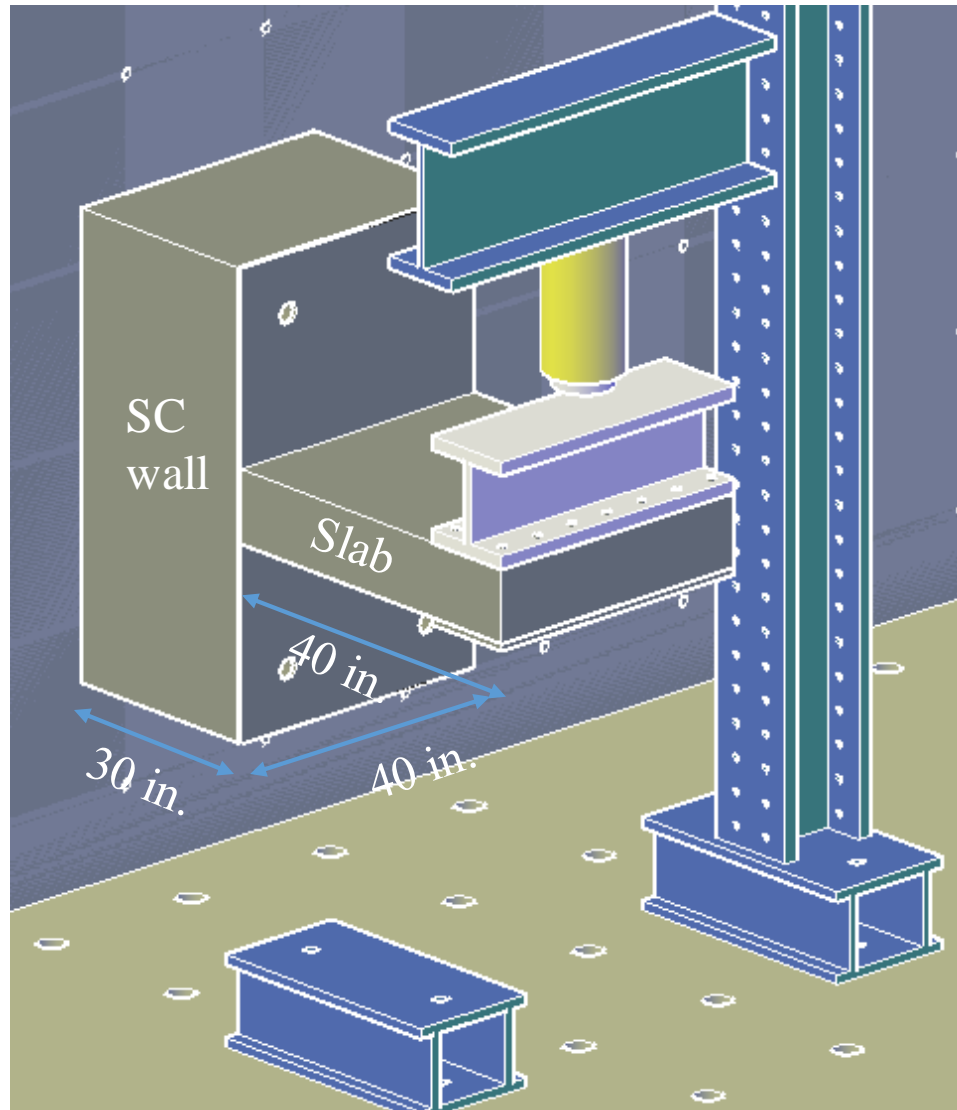
- Slab type : RC or half SC (HSC)
- Rebar : rebar type (Hooked bar or T headed rebar), Reinforcement ratio, Embedded length, and Rebar location in the SC wall portion



# SC SLAB-TO-WALL CONNECTION

## *Experimental Program*

- Test setup



# FINDINGS

- SC wall-to-wall T connection test
  - The joint shear failure mode for all test specimens
  - No significant effects of the shear reinforcement ratio and the steel headed stud layout
  - $V_{njs}^{TEST}$  within the range of 426.7 kips - 454 kips Greater than  $V_{njs}^{ACI-exp}$  (413 kips) by 3.1% - 10.6%
  - The ACI 349-06 (2006) code equation is applicable and conservative for estimating the joint shear strength of SC wall-to-wall T joints with  $\gamma$  of 12
- SC wall-to-wall L connection test
  - The joint shear failure mode
  - $V_{njs}^{TEST}$  of 261.7 kips close to  $V_{njs}^{ACI-exp}$  (262.7 kips)
  - The ACI 349-06 (2006) code equation is applicable for estimating the joint shear strength of SC wall-to-wall L joints with  $\gamma$  of 8

# Publications

- Seo, J., Varma, A.H., and Winkler, D. (2013). "Preliminary Investigations of the Joint Shear Strength of SC Wall-to-Wall T-Joints." Transactions of SMiRT 22, IASMIRT, NCSU, Raleigh, NC, pp. 1-10.  
[http://www.iasmirt.org/transactions/22/Pap\\_863\\_ver\\_3.pdf](http://www.iasmirt.org/transactions/22/Pap_863_ver_3.pdf)
- Seo, J., and Varma, A.H. (2015). "Behaviour and Design of Corner or L-Joints in SC Walls." Transactions of SMiRT 23 in Manchester, UK, Paper ID 695, IASMIRT, North Carolina State University, Raleigh, NC, pp. 1-10, [http://smirt23.uk/attachments/SMiRT-23\\_Paper\\_695.pdf](http://smirt23.uk/attachments/SMiRT-23_Paper_695.pdf)