

# Continuously Variable Series Reactor (CVSR) for Distribution System Applications

## TRAC Program Review

*US Department of Energy, Office of Electricity*

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*Oak Ridge National Laboratory*

**Presented at Oak Ridge National Laboratory**

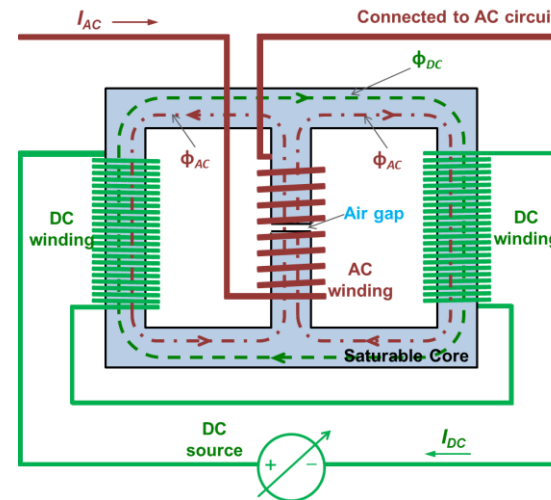
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August 13<sup>th</sup>, 2019

# Project Overview

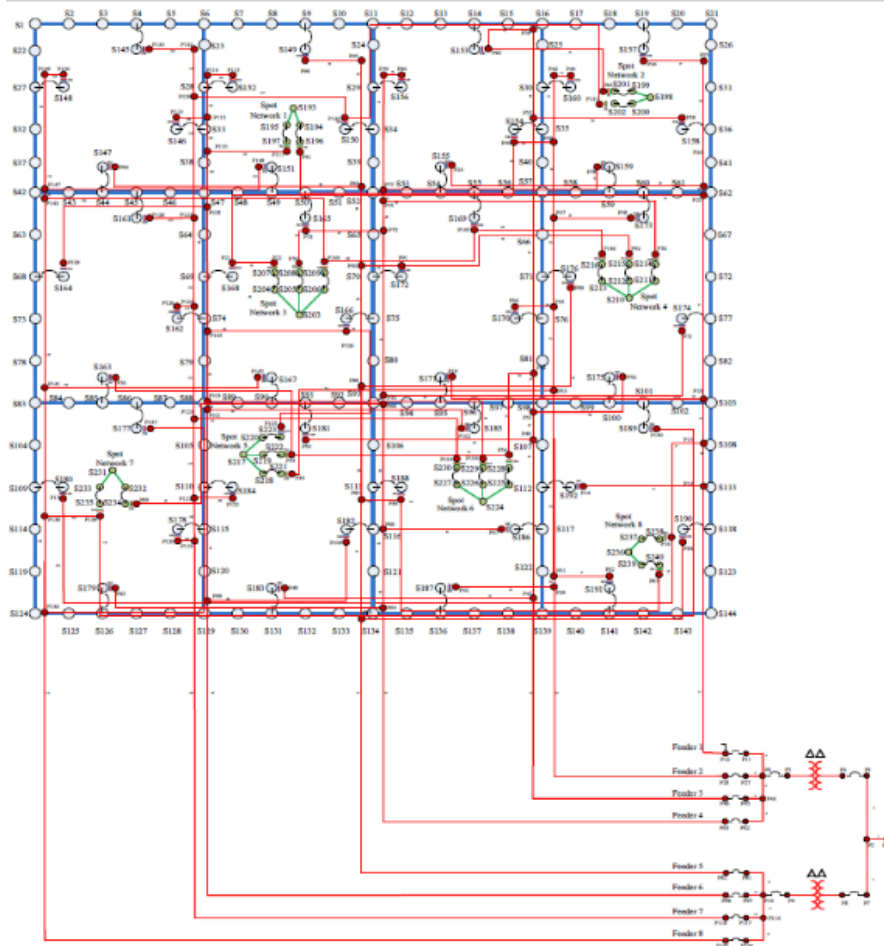
- Objective
  - ✓ CVSR concept extended to distribution grid applications
  - ✓ Preliminary studies facilitating future development and deployment
    - Use case
    - Valuation
    - Prototype
- DOE award: \$450k
- Duration: 18 months (01/19 – 06/20)
- Team
  - ✓ ORNL (lead)
  - ✓ UCF
  - ✓ UTK



Transmission level CVSR prototype from previous ARPA-e project

# Context concerning the problem being addressed

- Distribution system for metropolitan and suburban districts



- ✓ Configuration complexity
- ✓ High load density
- ✓ Restrict reliability requirements
- ✓ Increased complexity of power flow
- ✓ Insufficient PFC capability

## Need for power flow solutions

- Low cost/high reliability
- Meeting distribution system-specific requirements

# State of the art approaches

- Full/partial-rating power electronics (P.E.) based solutions, e.g., Grid Energy Router\*, modular control transformer



P.E. solutions



CVSR solution



\* Reference: NRECA report, "Field Demonstration: Grid Energy Router – Advanced Device for Voltage Control and Power Quality Management," February 2016. [https://www.cooperative.com/programs-services/bts/documents/reports/grid\\_energy\\_router\\_demo.pdf](https://www.cooperative.com/programs-services/bts/documents/reports/grid_energy_router_demo.pdf)

# Strategy and uniqueness of the proposed solution

## CVSR

- ✓ Proved in previous projects
- ✓ Analysis tools for design & optimization
  - FEA
  - MEC
- ✓ Lab-scale prototype for validation

## Use case

- ✓ Interests of utilities
- ✓ Standard models (easy for research) and real system models (reflecting real problems)
- ✓ Quantitative analysis
  - Power flow
  - Sensitivity analysis

## Valuation

- ✓ Cost assessment
- ✓ Quantitative analysis for economic benefits
  - Optimization
  - Placement
- ✓ Scalability

# Specific research questions being addressed

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- What are the problems in distribution grid possibly to be solved by using CVSR?
- What are the use cases best proving the values of the technology in the selected system models?
- How to determine the appropriate specifications for the identified use case?
- Identify potential issues in advance through prototype development.

# Significance of the results, if successful



## Representative Use Cases

Identify and solve problems in real systems



## Valuation

Boost stakeholders' confidence & facilitate technology adoption



## Analysis Framework

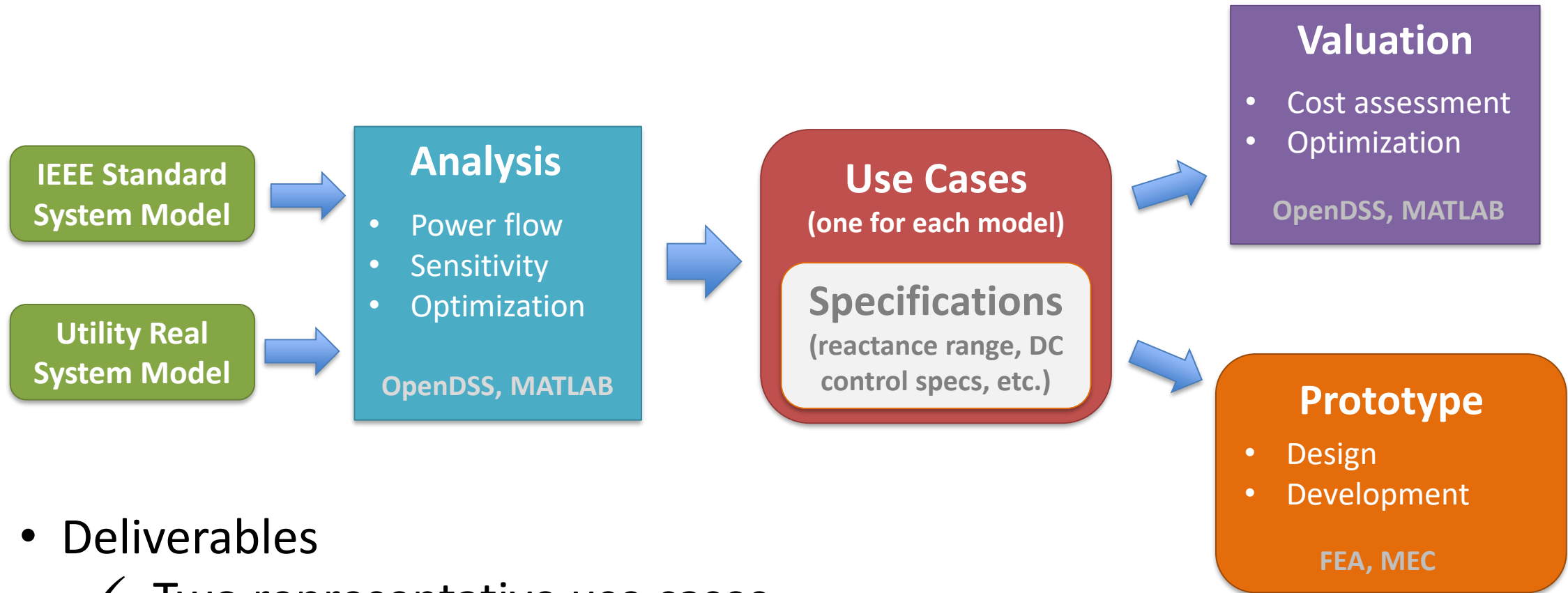
Help future R&D of the technology or similar



## Potential Issue Detection

Identify potential issues in advance to reduce risks

# Proposed approach



- Deliverables
  - ✓ Two representative use cases
  - ✓ Valuation study results
  - ✓ One lab-scale prototype



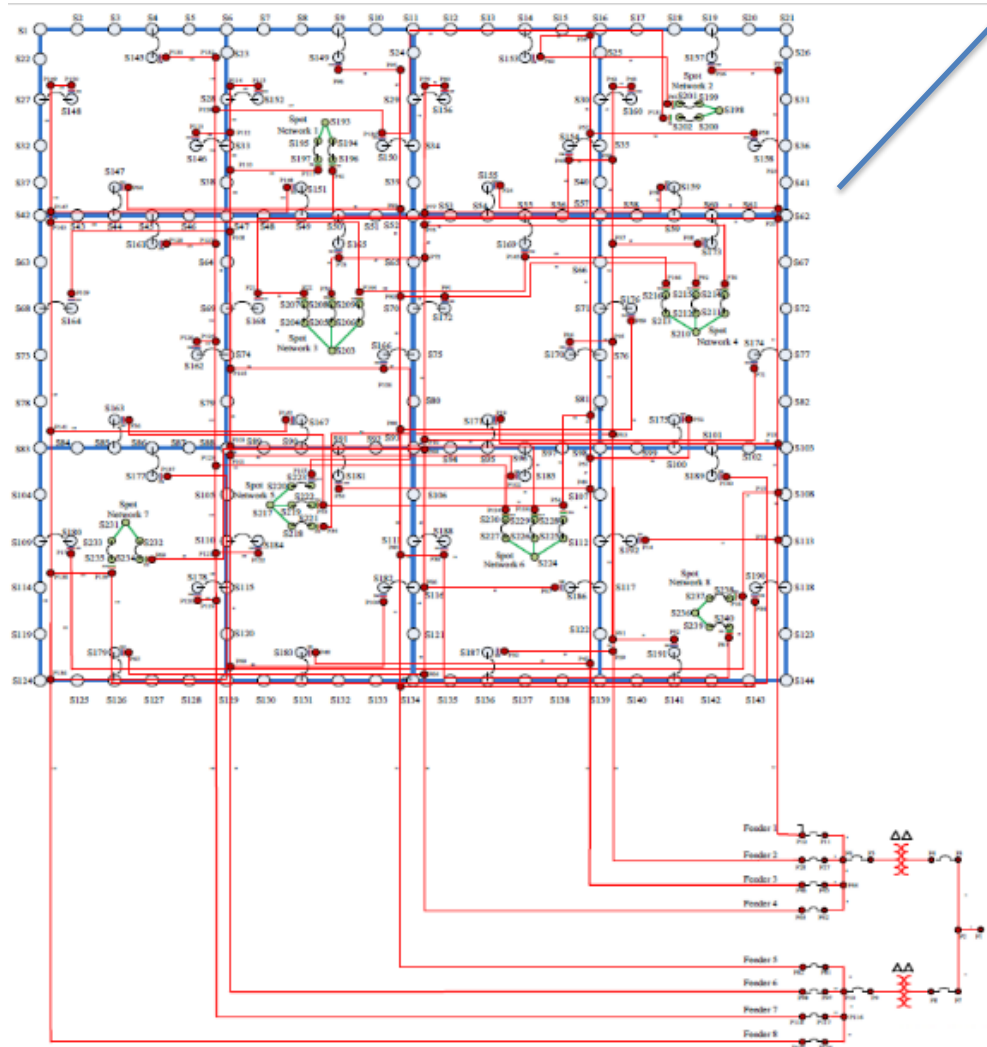
# Project tasks, schedule, and funding status

Task	FY19 Q2			FY19 Q3			FY19 Q4			FY20 Q1			FY20 Q2			FY20 Q3		
Task 1: Use case and device specifications	█	█	█															
Task 2: Modeling and design			█	█	█	█	█	█										
Task 3: Integration: optimal placement and valuation				█	█	█	█	█	█	█	█	█	█	█				
Task 4: Prototype development						█	█	█	█	█	█	█	█	█	█	█		
Task 5: Scalability study												█	█	█	█	█	█	

	Funds Remaining
ORNL	\$100k
UTK (@ end of April)	\$70.7k
UCF (@ end of August)	\$41k

# Progresses and results

- System models used for integration studies



## IEEE 342-node LVNTS

- 2 delta-delta step down transformers with 8x13.2 kV distribution feeders.
- Grid (meshed) and spot networks on secondary
- Secondary network transformers at 1 MVA rating, spot network transformers at 1.5, 2, and 2.5 MVA ratings.

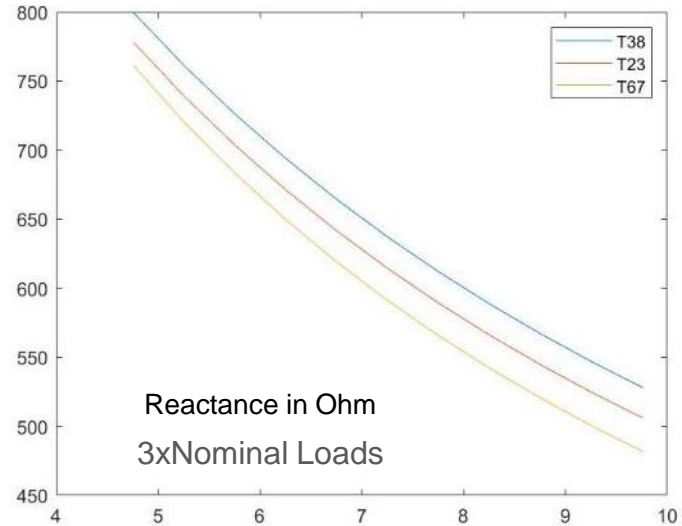
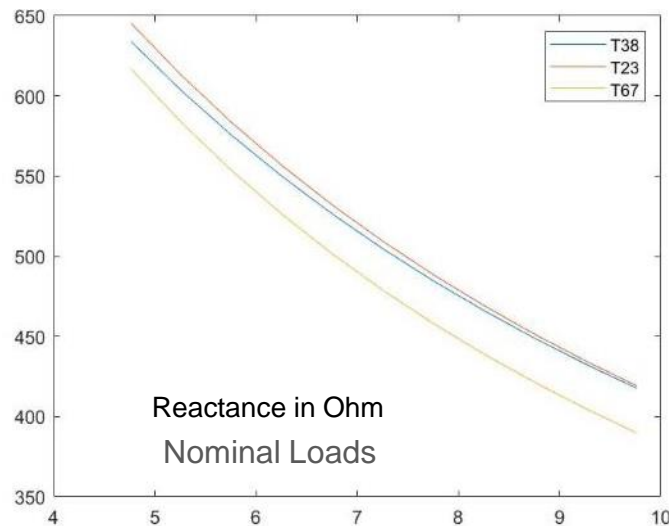
## ConEd distribution system model

- Waiting on NDAs

# Use case development - 1

## Loading sensitivity

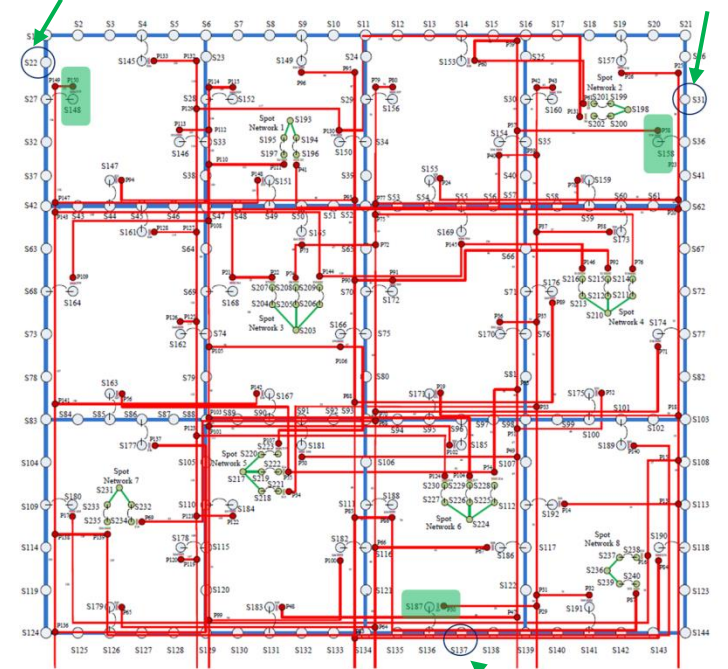
- Nominal loads at three nodes are increased by a factor of 3.
- Results show how transformers pick up the extra load and the proportion is very close to linear.
- To find out the vulnerable transformers



Power Flow on the Primary Side of Transformers

Total Load at S22=145 kVA

Total Load at S31=144.3 kVA



Total Load at S137=130.5 kVA

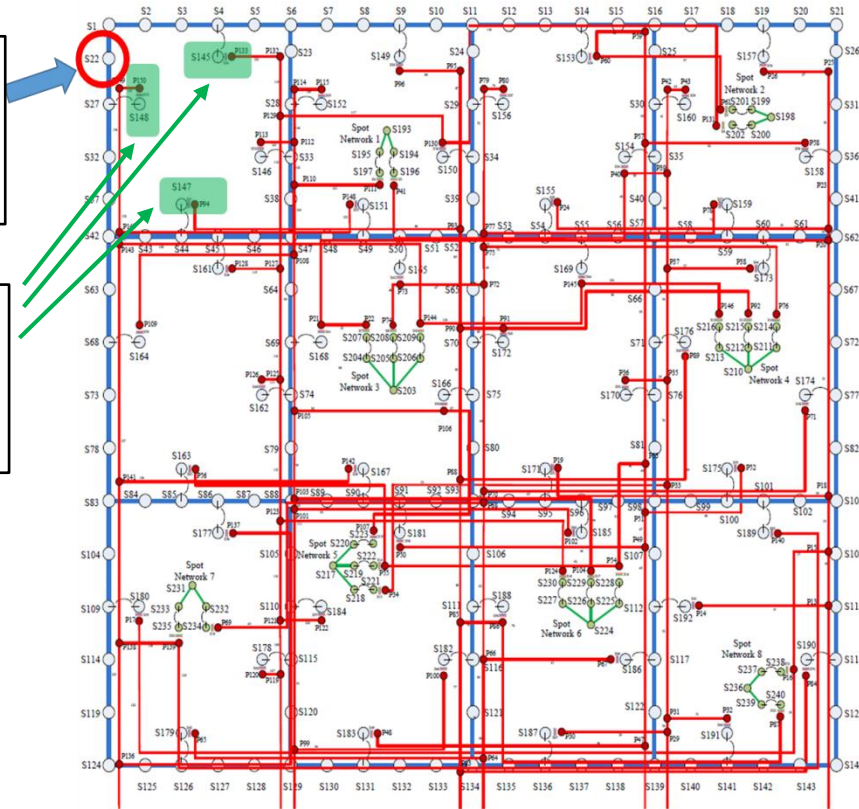
All transformers are secondary network transformers, and they are rated at 1MVA

# Use case development - 2

- Transformer loading relief when load @S22 significantly increased

Total load @ S22  
(145kVA)  
multiplied by 8

3 transformers  
nearby  
considered



- ✓ Use CVSR to keep transformers T23, T24, and T31 from overloading.
- ✓ Simulation results are obtained through OpenDSS-MATLAB

# Use case development - 3

- Determine optimal reactance value(s) of CVSR

## Case 1: Use one CVSR unit

Case 1: Only T-23 has CVSR device						
S22	T-23		T-24		T-31	
	kVA	ohm	kVA	ohm	kVA	ohm
Coefficient = 8	1132	4.76	945.3	4.76	728.3	4.76
	1076	5.26	960.6	4.76	740.2	4.76
	1024	5.76	974.3	4.76	750.9	4.76
	977.4	6.26	986.9	4.76	760.7	4.76
	934.2	6.76	998	4.76	769.5	4.76
	894.5	7.26	1008	4.76	777.5	4.76

## Case 2: Use two CVSR units

Case 2: T-23 and T-24 have CVSR device						
S22	T-23		T-24		T-31	
	kVA	ohm	kVA	ohm	kVA	ohm
Coefficient = 8	1132	4.76	945.3	4.76	728.3	4.76
	1088	5.26	914.3	5.26	743.2	4.76
	1046	5.76	884.8	5.76	757.1	4.76
	1008	6.26	856.6	6.26	769.8	4.76
	971.1	6.76	829.5	6.76	781.5	4.76
	936.9	7.26	803.88	7.26	792.3	4.76
	904.9	7.76	779.4	7.76	802.3	4.76
	874.6	8.26	756.1	8.26	811.6	4.76

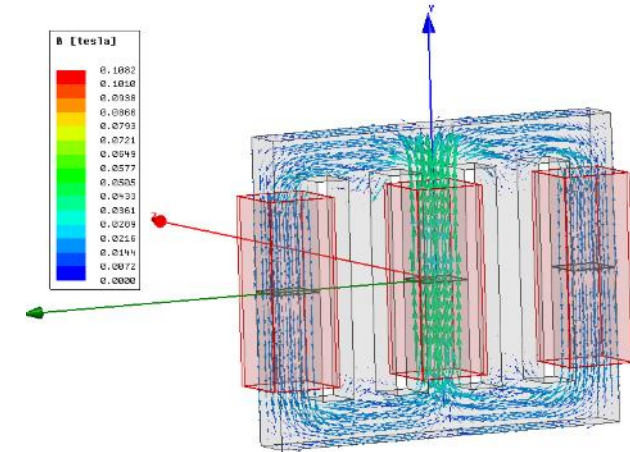
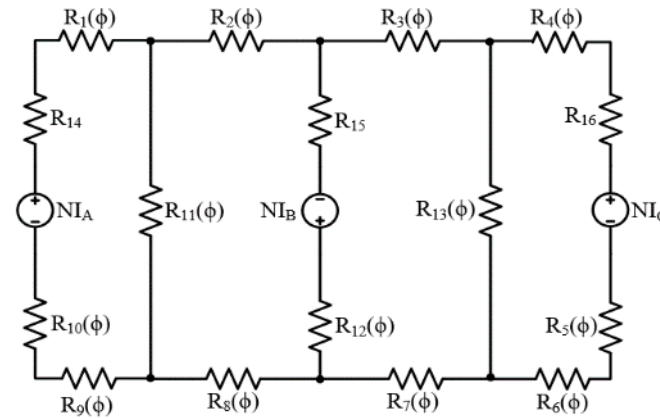
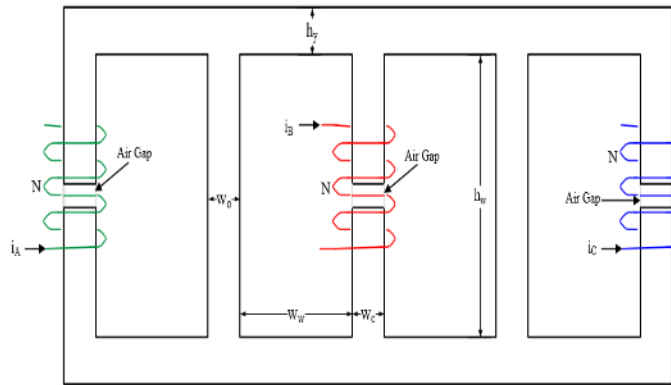
# Use case development - 4

- Linear optimization analysis and comparison with OpenDSS

Case 1: Only T-23 has CVSR device						
S22	T-23		T-24		T-31	
Coefficient = 8	kVA	ohm	kVA	ohm	kVA	ohm
Optimization Result from MATLAB (Linprog)	1000	6.096	980.48	4.76	755.76	4.76
OpenDSS (Benchmark)	992.31	6.096	982.82	4.76	757.55	4.76
Relative Error in Percent	0.774%	--	0.238%	--	0.236%	--

# CVSR device modeling - 1

- Modeling of CVSR by using analytical and numerical methods
- For designing the lab-scale prototype



## Magnetic Equivalent Circuit (MEC) method

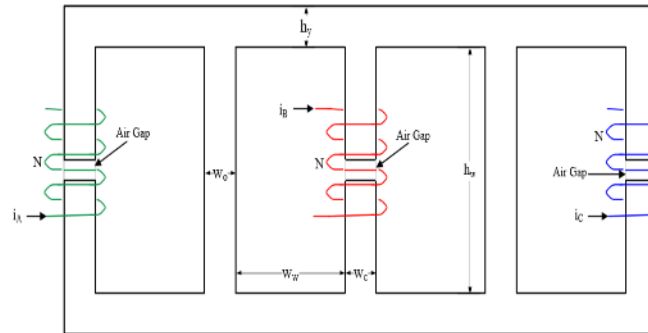
## Finite Element Analysis (FEA) method

One example for analysis:

- 13.8kV, 500kVA transformers
- Phase current  $\sim 30A$

# CVSR device modeling - 2

- Configuration design and reactance regulation of 3-phase device



\* G = Gap  
 $N_{ac} = 42$   
 $N_{dc} = 39$

**Config. #1**

	1 (G)	2	3 (G)	4	5 (G)
DC MMF	0	$N_{dc}I_{dc}$	0	$N_{dc}I_{dc}$	0
AC MMF	$N_{ac}I_a$	0	$N_{ac}I_b$	0	$N_{ac}I_c$

**Config. #2**

DC MMF	$N_{dc}I_{dc}$	$-1.5N_{dc}I_{dc}$	$N_{dc}I_{dc}$	$-1.5N_{dc}I_{dc}$	$N_{dc}I_{dc}$
AC MMF	$N_{ac}I_a$	0	$N_{ac}I_b$	0	$N_{ac}I_c$

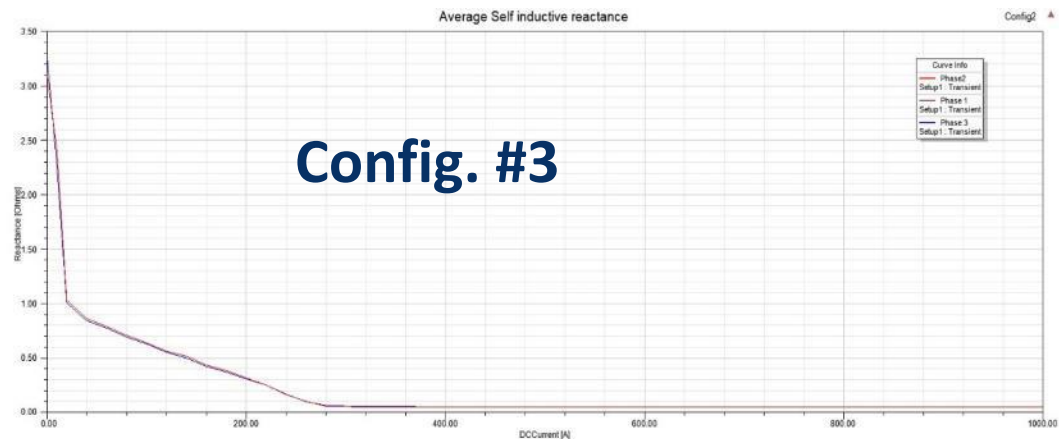
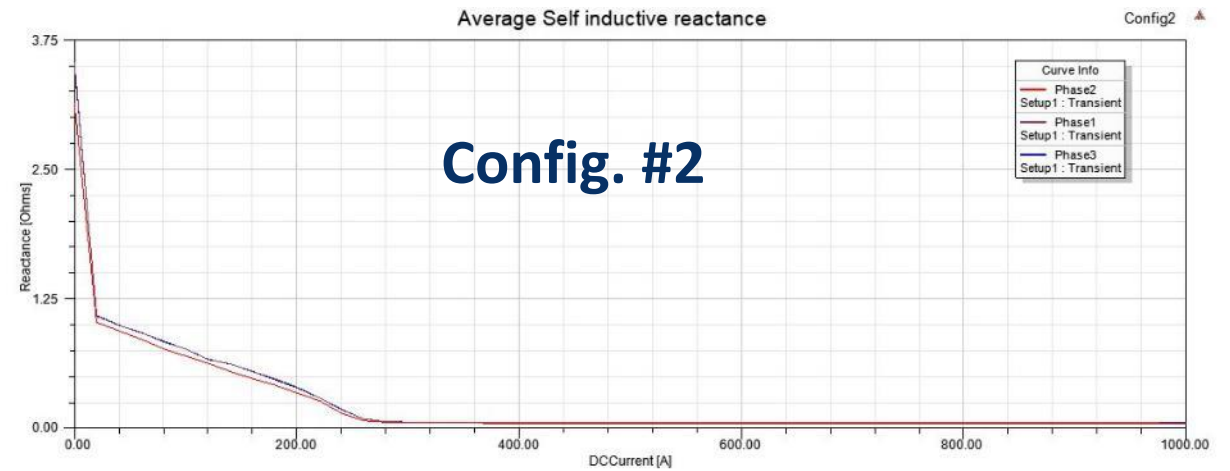
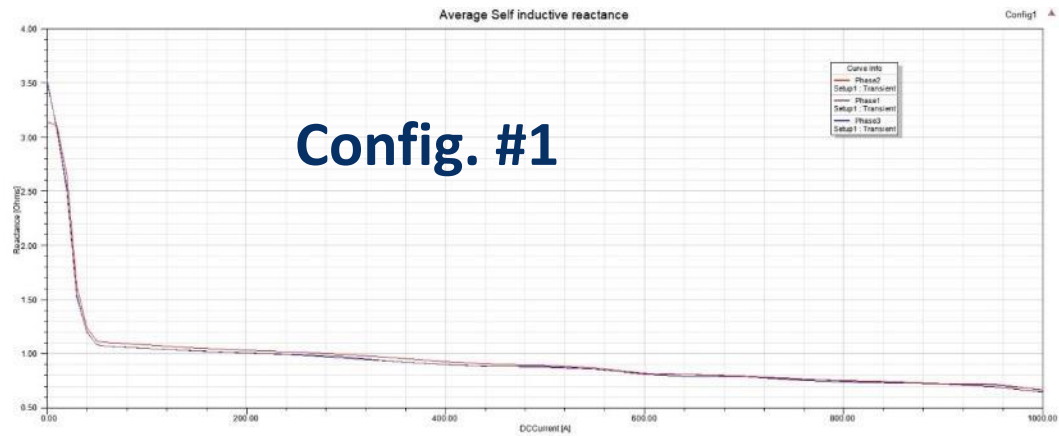
**Config. #3**

DC MMF	$-1.5N_{dc}I_{dc}$	$N_{dc}I_{dc}$	$N_{dc}I_{dc}$	$N_{dc}I_{dc}$	$-1.5N_{dc}I_{dc}$
AC MMF	0	$N_{ac}I_a$	$N_{ac}I_b$	$N_{ac}I_c$	0



# CVSR device modeling - 3

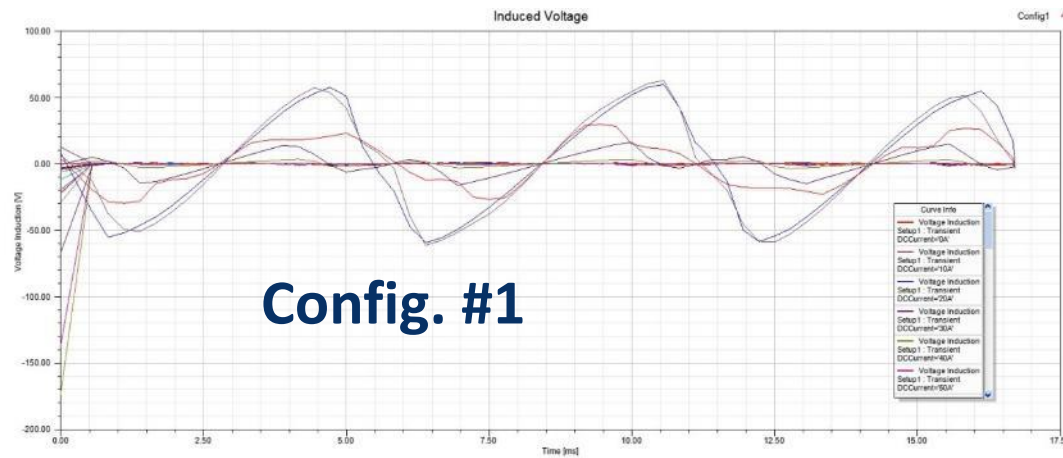
- Configuration design and reactance regulation of 3-phase device



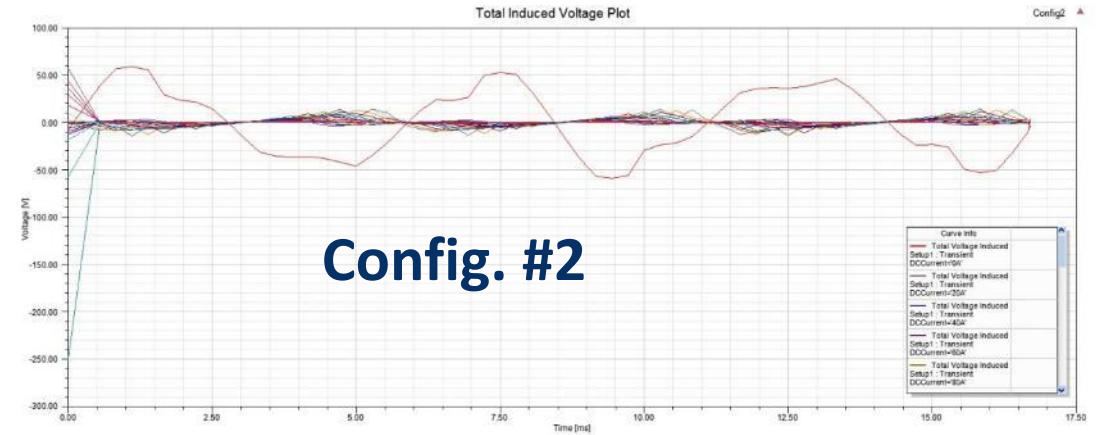
**Reactance regulation range  
(reactance vs. DC)**

# CVSR device modeling - 4

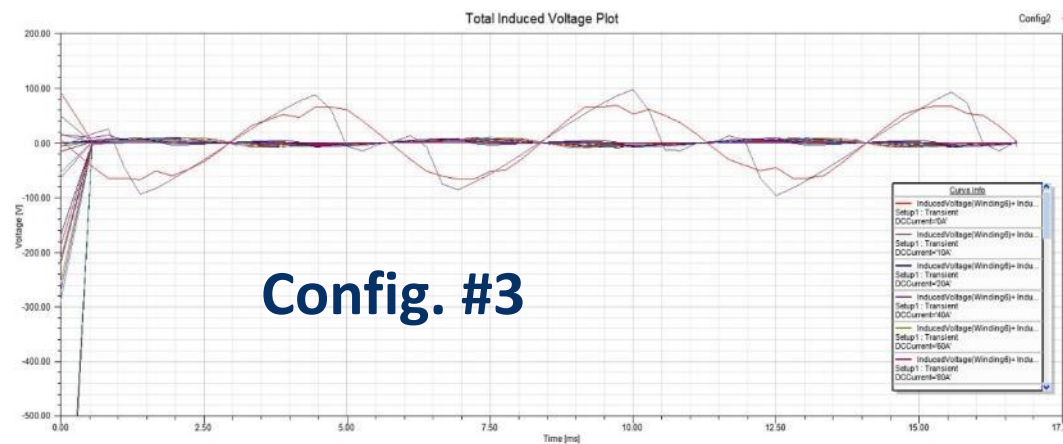
- Configuration design and reactance regulation of 3-phase device



**Config. #1**



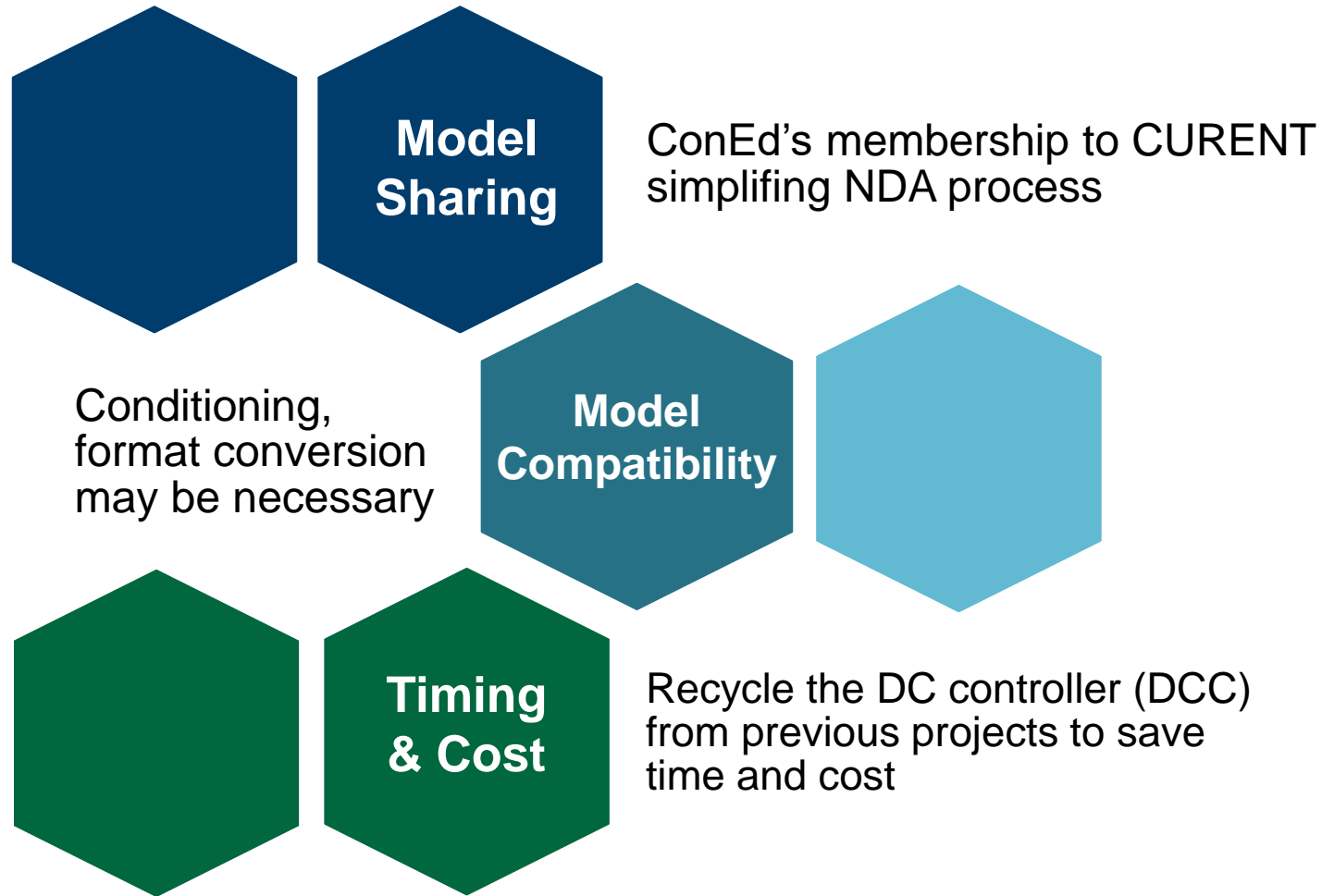
**Config. #2**



**Config. #3**

- ✓ #2 and #3 are better than #1 in terms of reactance range.
- ✓ #3 has larger induced voltage on DC winding compared to the other two (200V pk-pk vs. 120V pk-pk)

# Anticipated challenges and risk mitigation strategies



# Next steps

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- Conduct use case development for ConEd system once the model is available
- Conduct cost assessment and valuation by optimization analysis
- Determine the optimal design of core and winding configurations for the CVSR prototype
- Improve MEC model by considering saturation, for validation
- Preparing technical reports and publications.

# Broader Impact

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- Facilitating research on similar technologies to be used in distribution systems
- Pave the road to development of device for real system applications
- Boost utilities' confidence of CVSR applications in distribution network

# Contact Information

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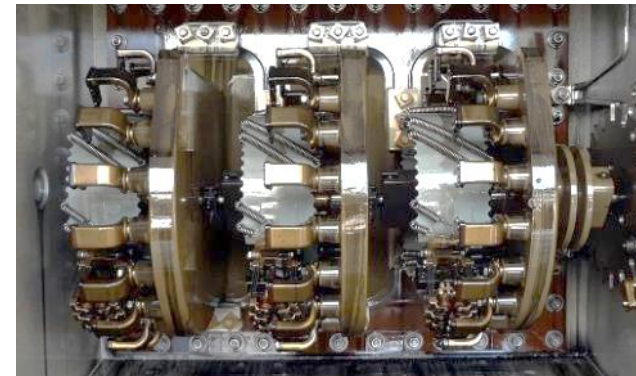
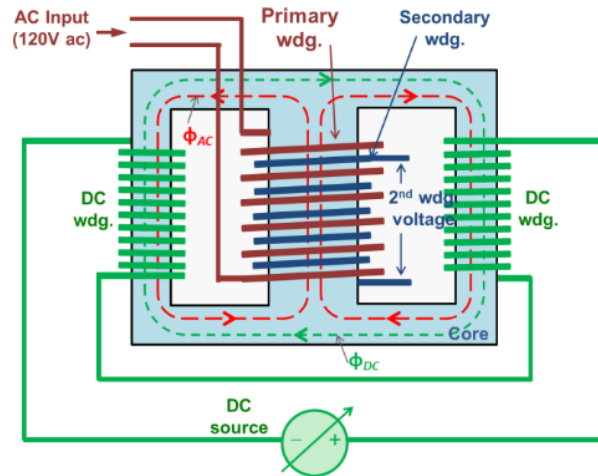
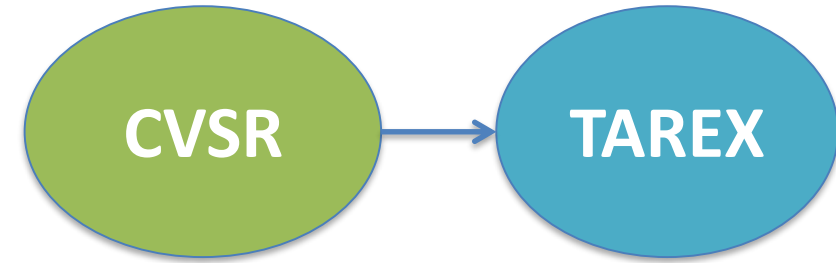
- ORNL: Dr. Zhi Li, [liz2@ornl.gov](mailto:liz2@ornl.gov)
- UCF: Prof. Aleksandar Dimitrovski, [ADimitrovski@ucf.edu](mailto:ADimitrovski@ucf.edu)
- UTK: Prof. Kevin Tomsovic, [tomsovic@tennessee.edu](mailto:tomsovic@tennessee.edu)

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# Updates on TAREX Project

## Tapless Regulating Power Transformer (TAREX)

- CVSR concept extended to transformer
- Magnetically regulated transformer voltage
- To replace mechanical tap changer



## Project Status

- Close to completion
- Final report being prepared, one invention disclosure being filed



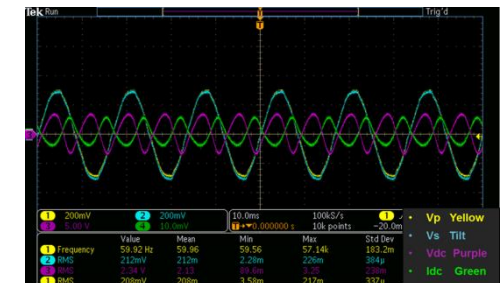
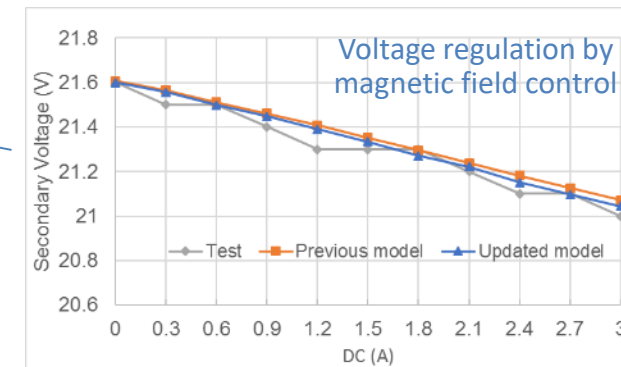
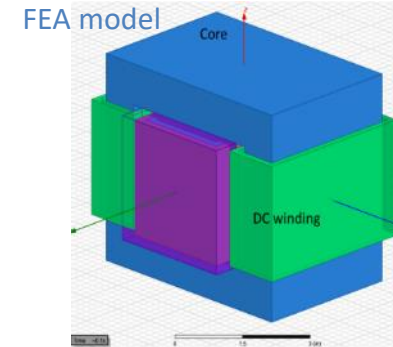
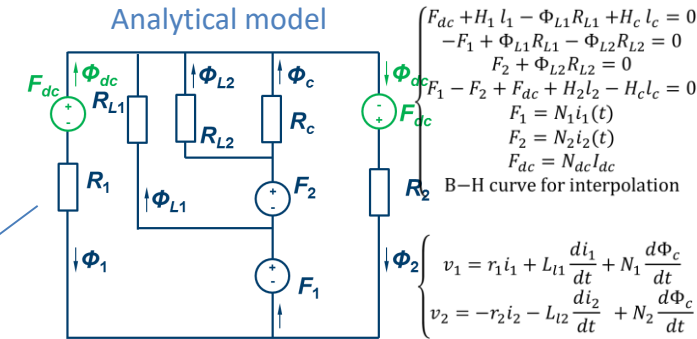
# Overview

## Objective

- To understand physics of TAREX and prove the concept

## Accomplishments

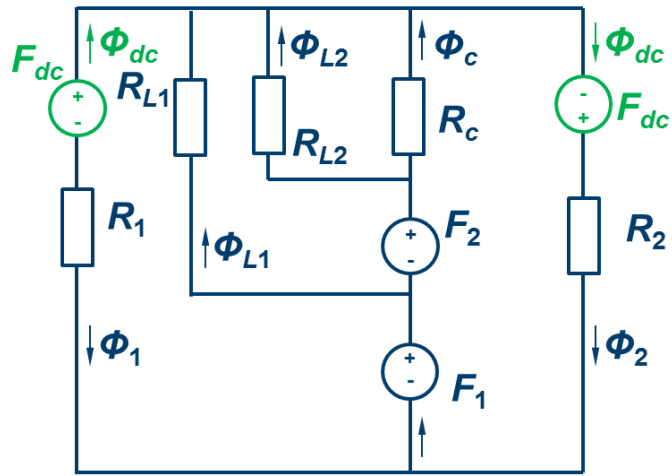
- Modeling** – multiple analysis models successfully developed and TAREXs' mechanism well understood
- Demonstration** – for the first time, demonstrated the magnetically regulated voltage of a transformer
- Validation** – validated the developed analysis models on a bench-top prototype
- Deliverables** – a comprehensive and validated approach to the analysis of TAREX for future projects



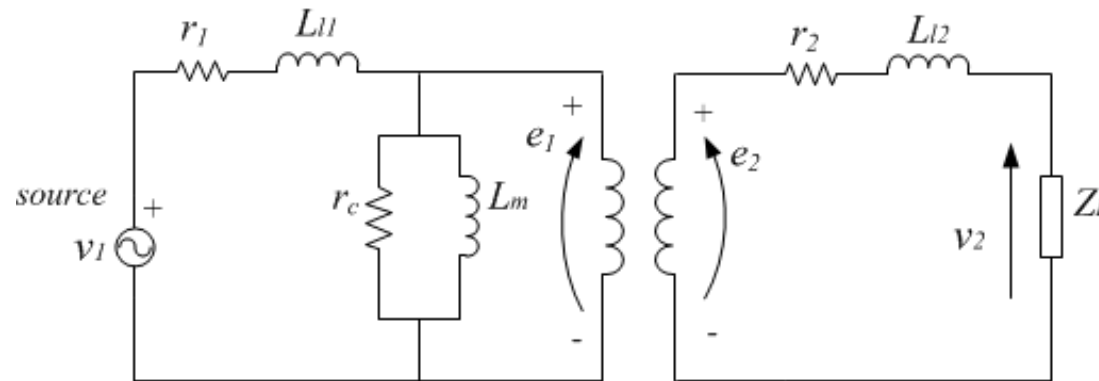
Bench-top prototype and testing

# Results - 1

- An analytical model developed and validated for modeling voltage regulation under dc biased magnetization
  - ✓ Considering dynamics in all three windings (primary, secondary, and dc)
  - ✓ Improved material characteristics based on testing results

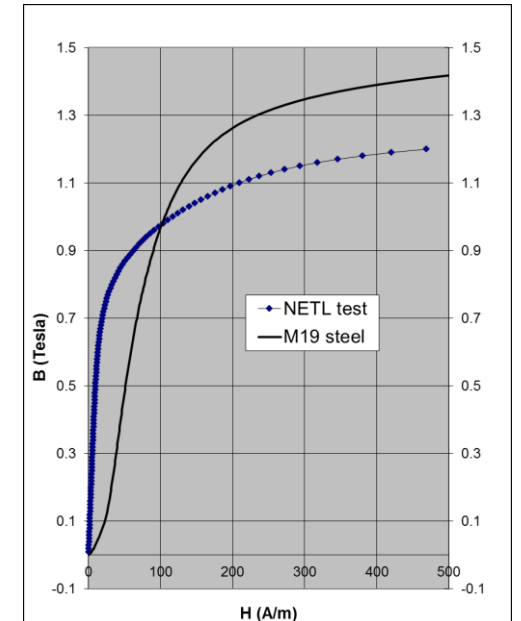
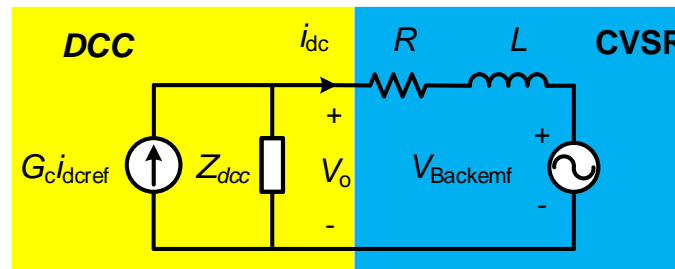


MEC model



Circuit model

DCC model

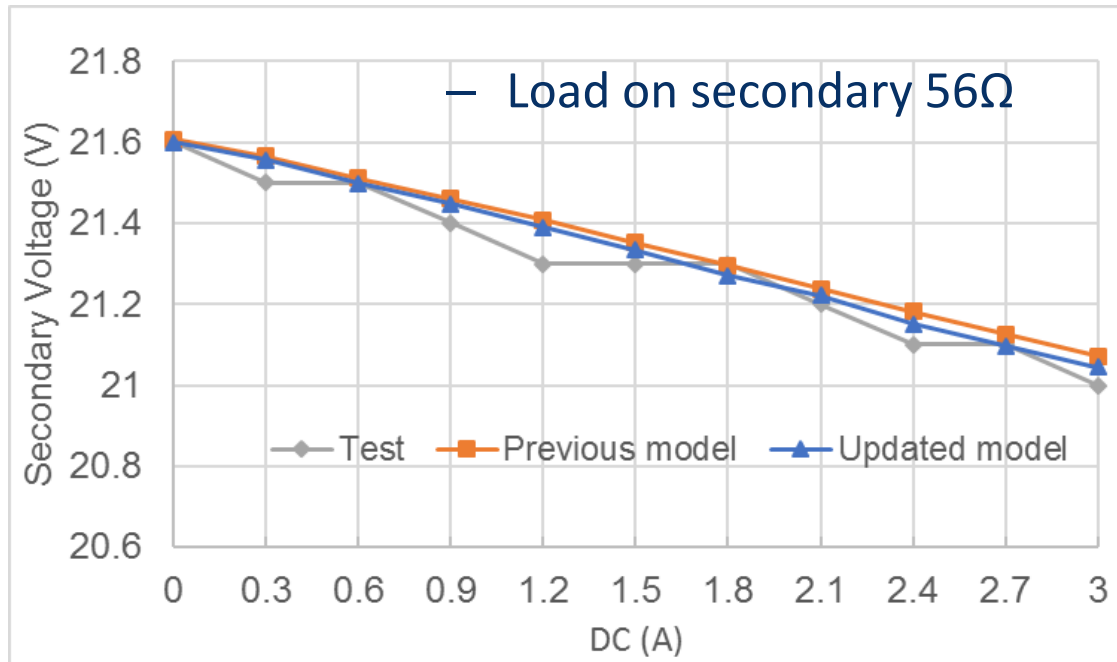


B-H curve from test

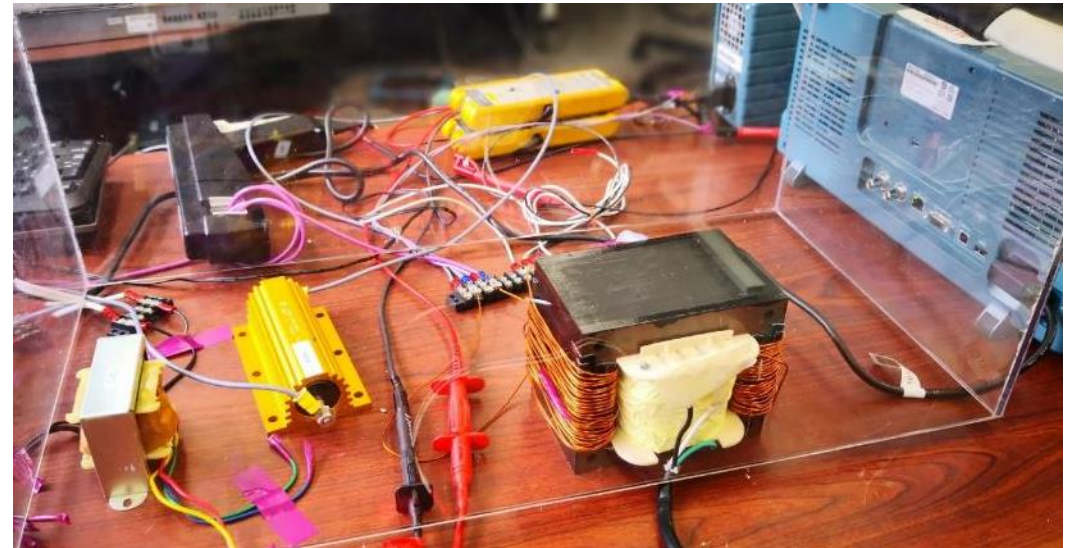
# Results - 2

- 115V/115V, 500VA prototype developed for validation

## Voltage regulation



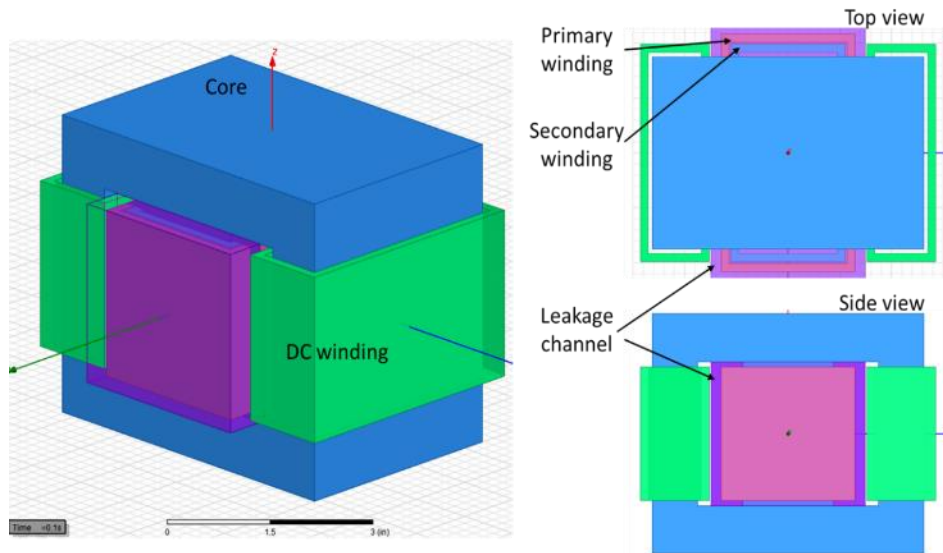
## Prototype testing setup



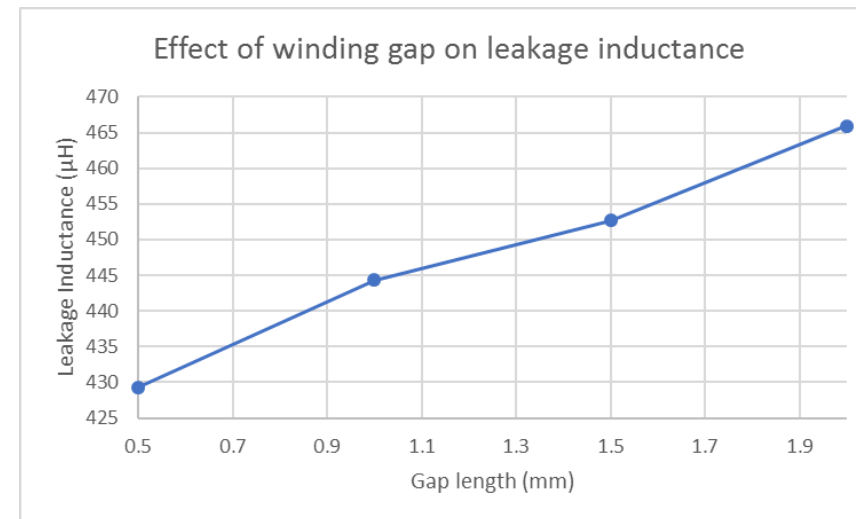
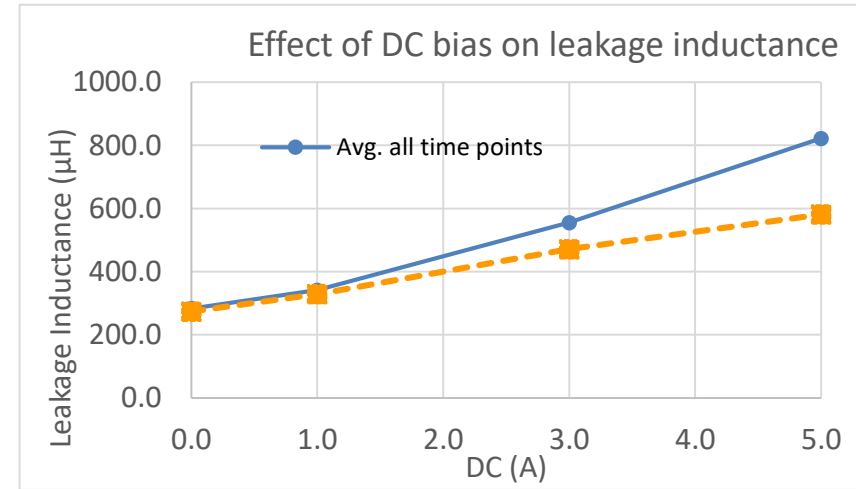
# Results - 3

- Leakage inductance modeled and analyzed

$$W = \frac{1}{2} L_l I^2 = \frac{1}{2\mu_0} \int_{leakage\ channel} B^2 dV$$



**FEA method to calculate leakage**



# Conclusion

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- DC-biased magnetization can be used to regulate winding voltage of transformers
- The voltage regulation is the consequence of a number of electromagnetically coupled processes, including magnetic induction, saturation, change of leakage inductance, etc.
- Leakage inductance is affected by DC bias in the core and geometry of the windings
- Only small range of voltage regulation is realized on the prototype. To reach larger range of regulation, the transformer should be carefully designed

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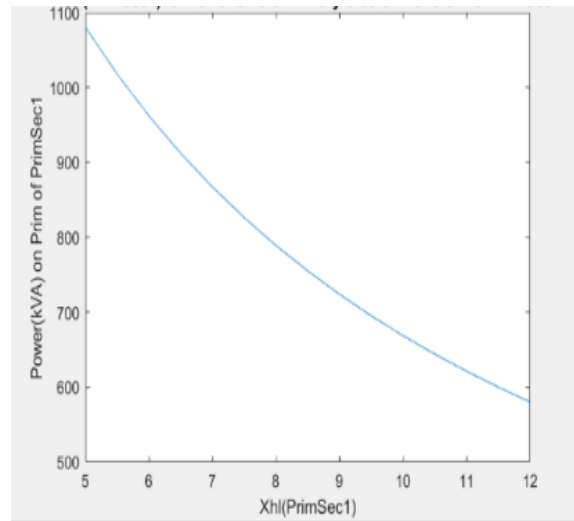
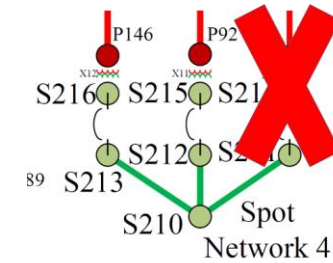
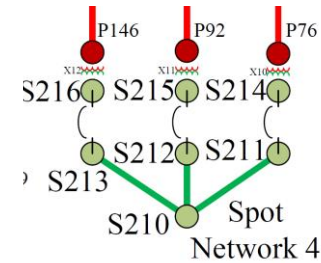
# Backup

# Backup slides

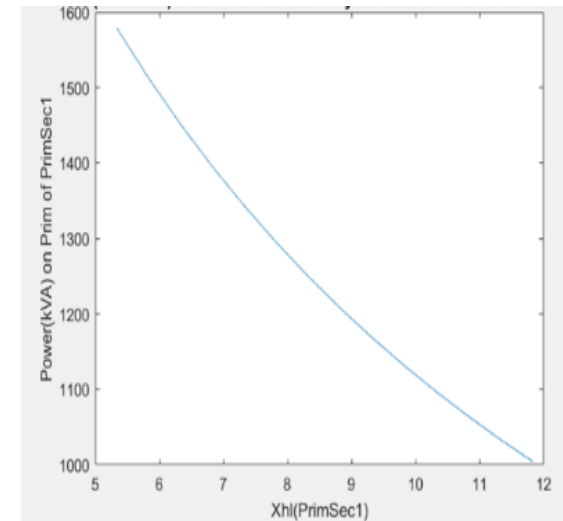
- Transformer overloading studies:

## Transformer outages

- Remove spot network Transformer-10
- Transformer-11 supplies the extra power, and its reactance affects the power flow.



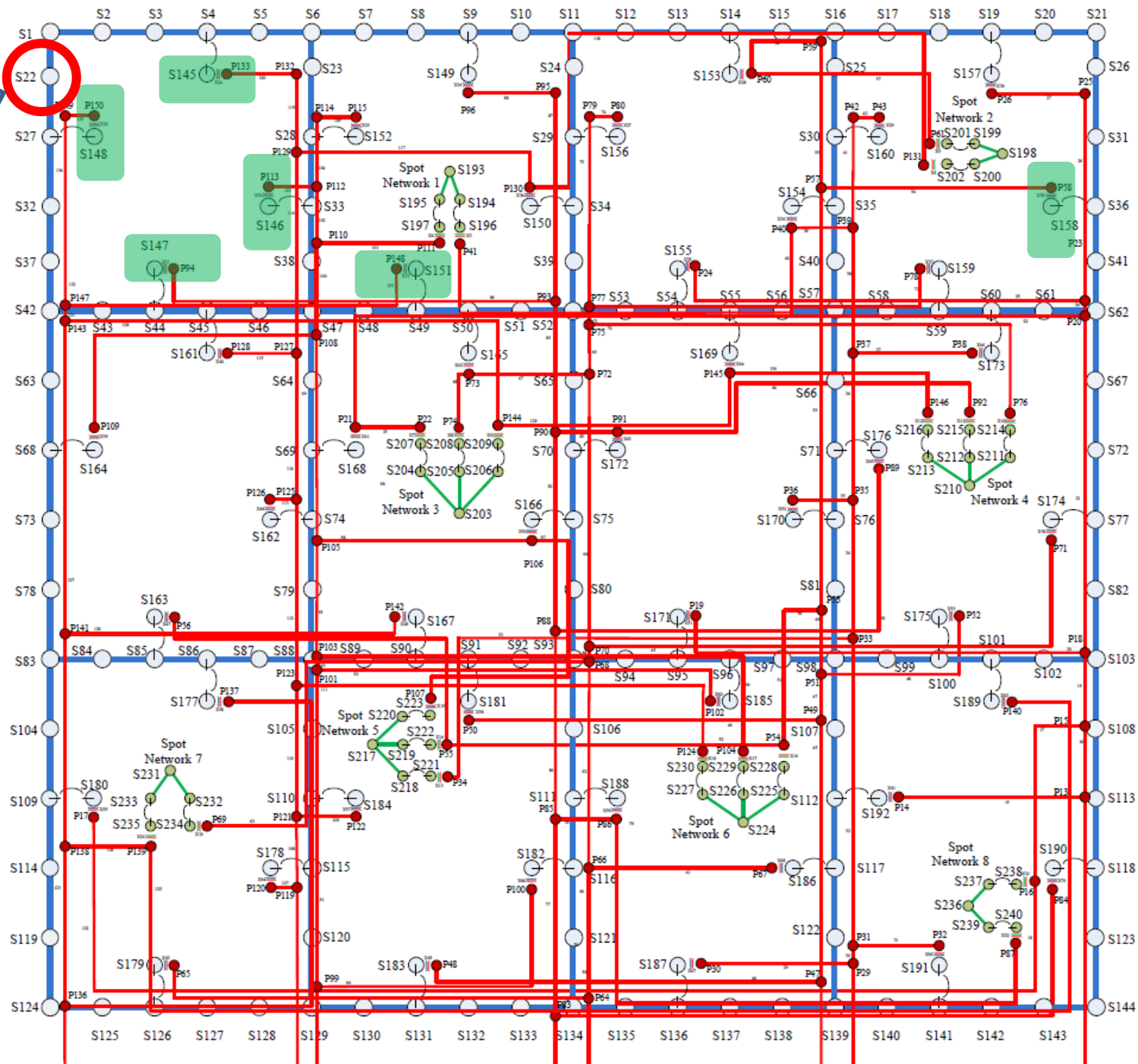
T11 - Base



T11 (T10 is removed)

Total Load at **S22=145 kVA**  
Increment rate is: **1:1.5:6**

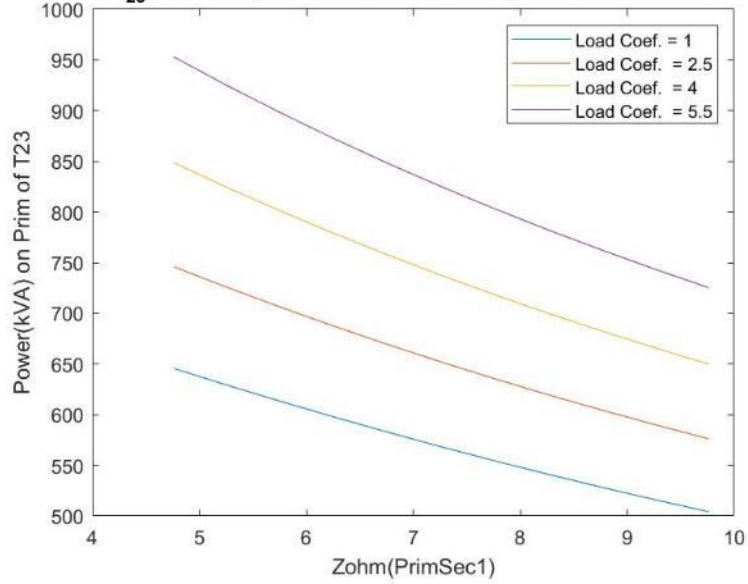
All Transformers are Secondary Network Transformers, rated at 1mVA



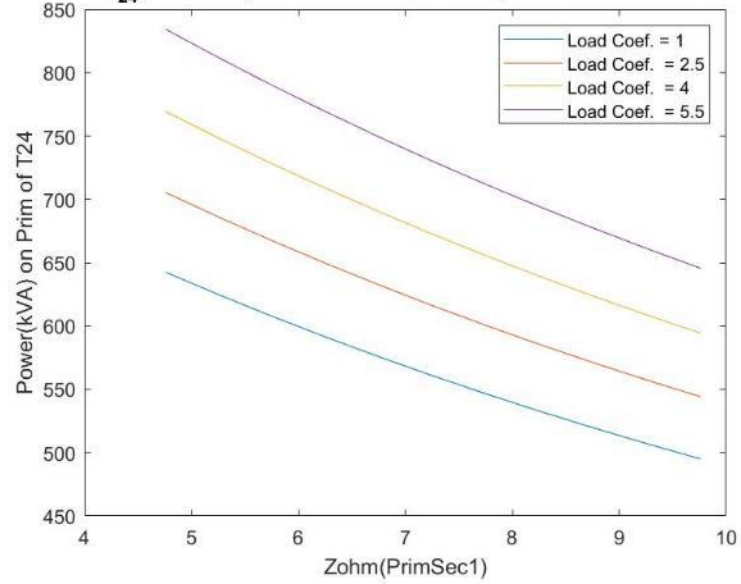


# Some Simulation Results

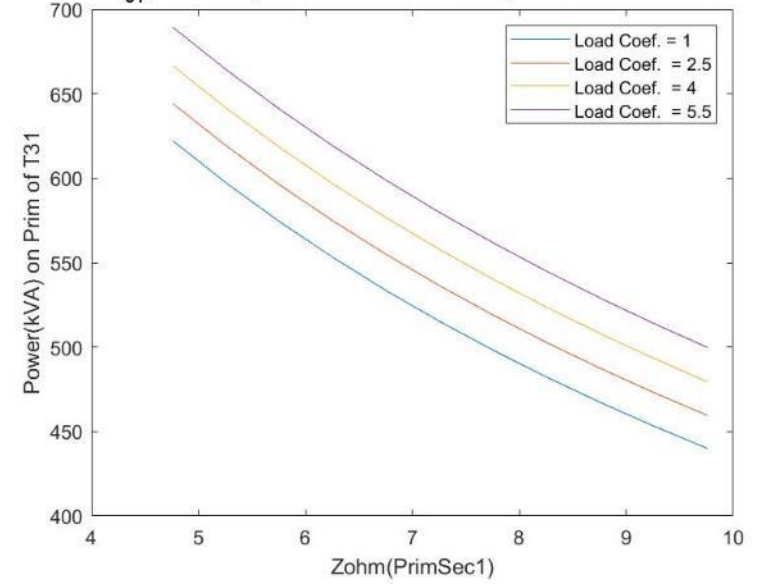
Zohm<sub>23</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.23



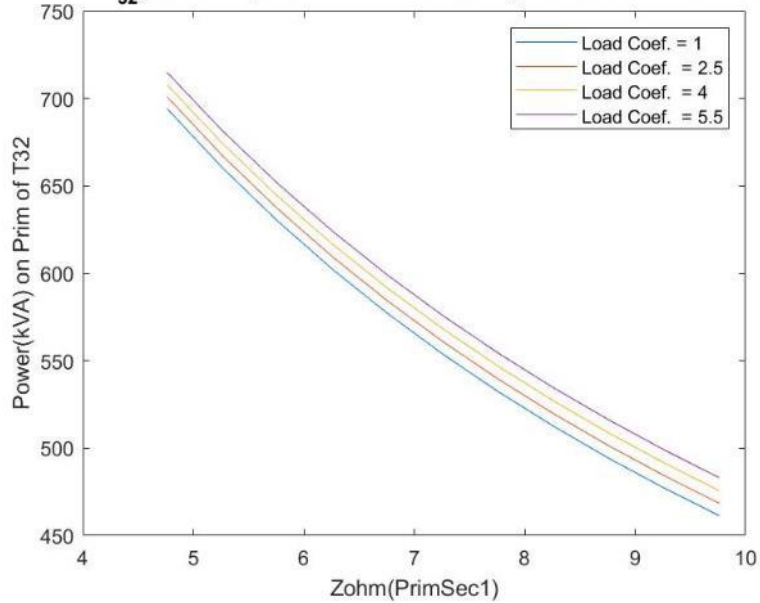
Zohm<sub>24</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.24



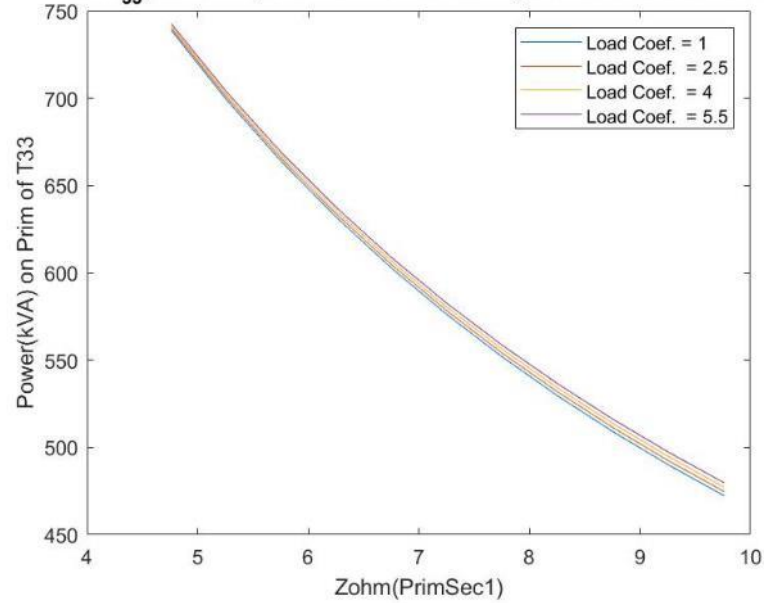
Zohm<sub>31</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.31



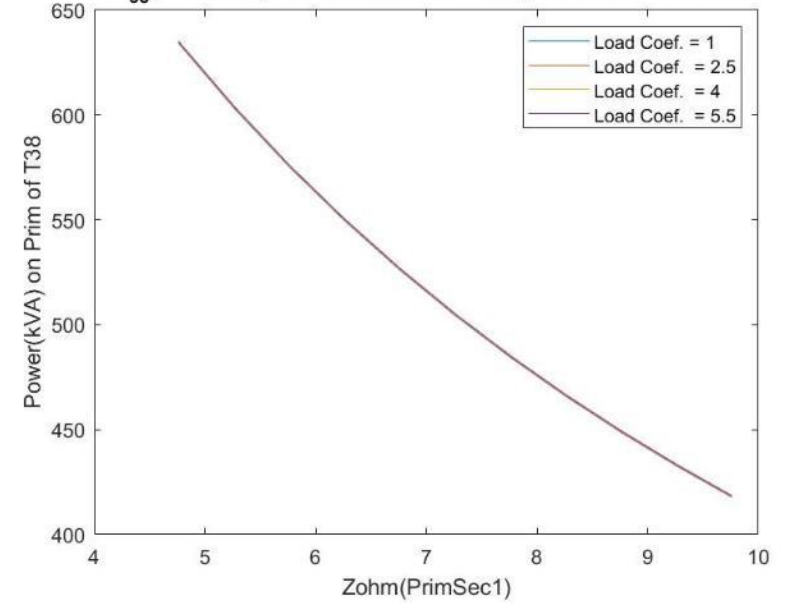
Zohm<sub>32</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.32



Zohm<sub>33</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.33



Zohm<sub>38</sub>(PrimSec1) vs. Power on the Primary Side of Transformer.38



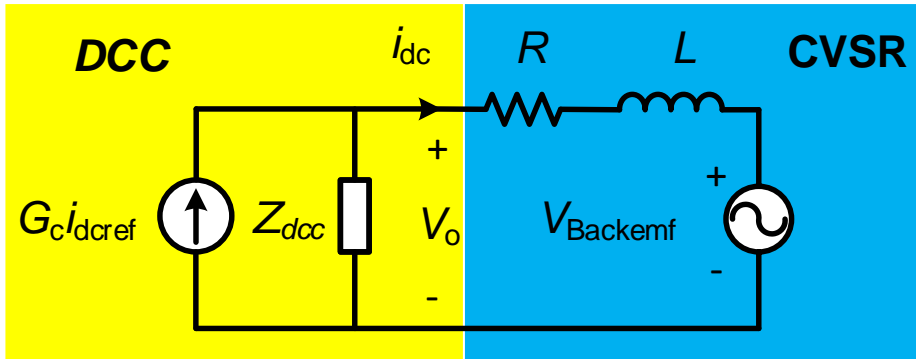
# Backup slides

- CVSR parameters for the 3-ph FEA model

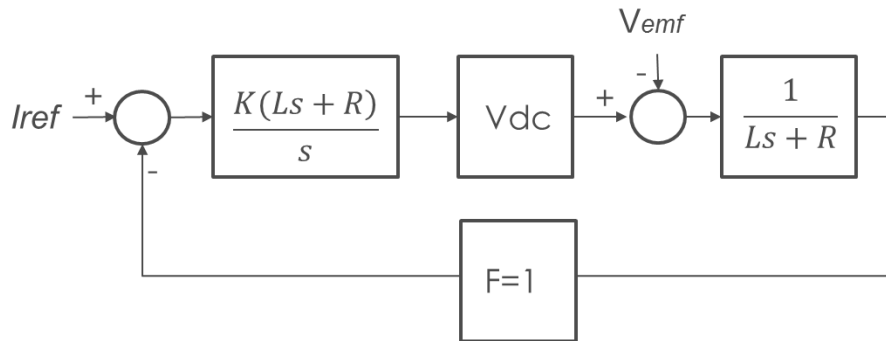
Parameters	Symbol	Value
Core height	$h_c$ (in)	20.72
Window height	$h_w$ (in)	14.72
Window width	$w_w$ (in)	2.2
Air Gap	$g$ (in)	0.06
Leg width	$w_c = w_o$ (in)	3
Core depth	$d_c$ (in)	3
Relative Permeability of core (Silicon Steel M36)	$\mu_r$	26673

# Backup slides - TAREX

- DCC model integration



time-domain  $Ri_{dc}(t) + L \frac{d[i_{dc}(t)]}{dt} + V_{emf} = 0$



s-domain  $i_{dc}(s) = G_1(s) \cdot I_{ref} + G_2(s) \cdot V_{emf}(s)$

