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# Cryo-Compressed Hydrogen Storage: Performance and Cost Review

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Compressed and Cryo-Compressed  
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# Cryo-Compressed Hydrogen Storage: Performance and Cost Review

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## ■ Contributors to the study

- LLNL: Gen2 and Gen3 design data, Aceves and Berry
- Argonne: On-board and off-board performance modeling, bill of materials, off-board cost modeling
- TIAX: On-board cost modeling

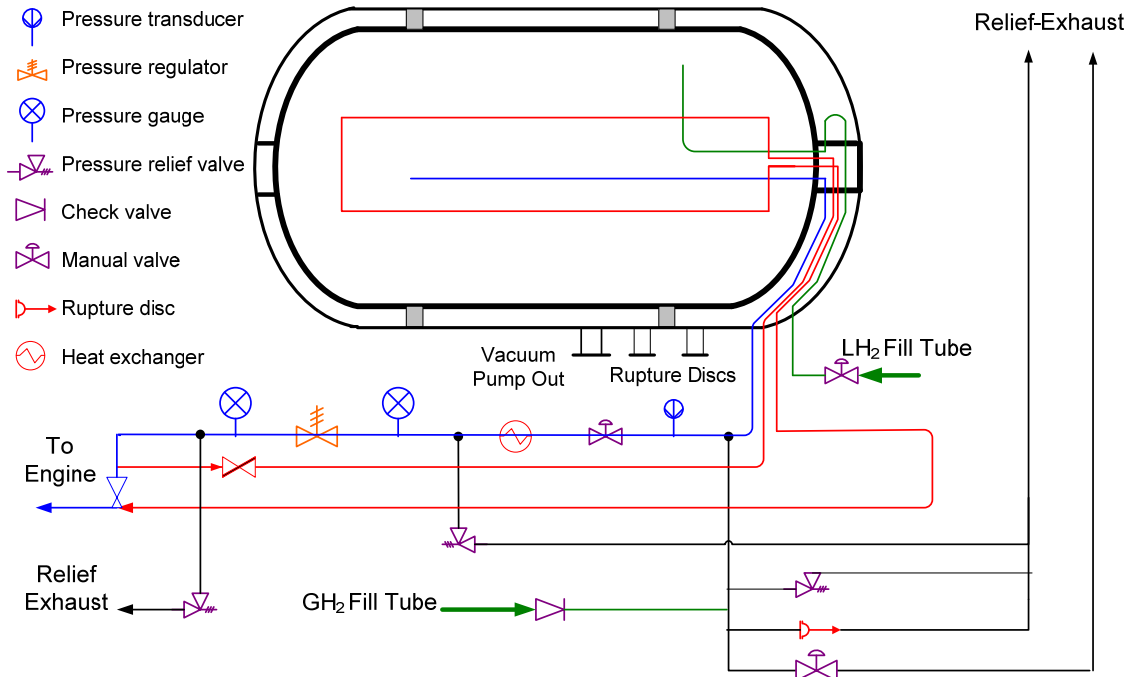
## ■ Results

- Gravimetric and volumetric capacity
- Refueling dynamics
- Discharge dynamics
- Dormancy and boil-off losses
- WTT efficiency
- Greenhouse gas emissions
- Storage system cost
- Refueling and ownership cost

# LLNL Gen3 Cryo-Compressed H<sub>2</sub> Storage System

## Modifications from Gen2

- Reduced insulation
- Better packaging
- Vacuum valve box eliminated
- In-tank heat exchanger
- 4000-psi pressure vessel rating



- System Volume: 235 L
  - Storage: 151 L
  - Vessel: 224 L
  - Ex-Vessel: 11 L
  - V Efficiency: 64.3%
- System Weight: 144.7 kg
  - LH<sub>2</sub> Stored: 10.7 kg
  - CH<sub>2</sub> Stored: 2.8 kg
  - Vessel: 122.7 kg
  - Ex-Vessel: 22.0 kg
- System Volumetric Capacity
  - 44.5 kg/m<sup>3</sup>: 1.5 kWh/L
  - LH<sub>2</sub> density: 70.9 kg/m<sup>3</sup> at 20.3 K, 1 atm
  - CH<sub>2</sub> density: 18.8 kg/m<sup>3</sup> at 300 K, 272 atm
- System Gravimetric Capacity
  - 7.1 wt%: 2.3 kWh/kg

# System Analysis of Physical Storage Systems

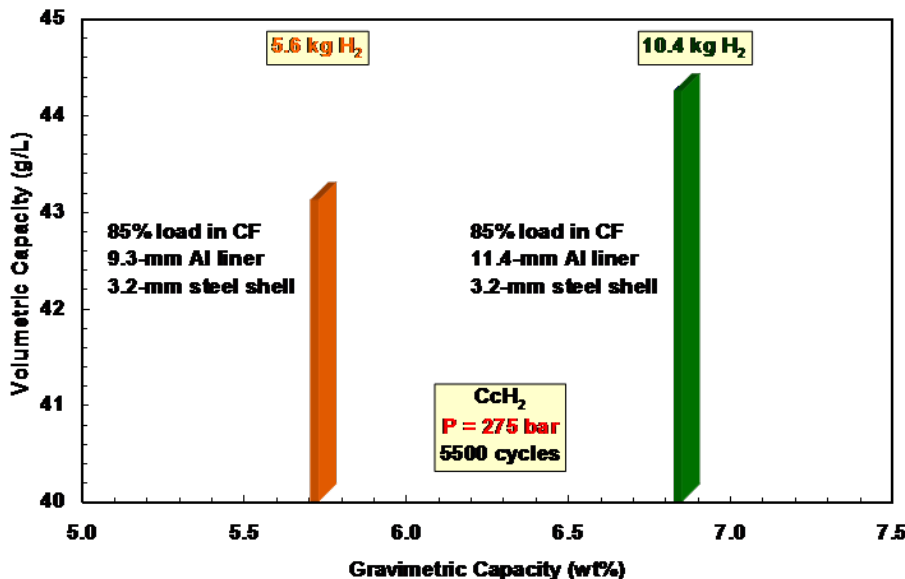
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- Benedict-Webb-Rubin equation of State: REFPROP coupled to GCtool
- Carbon Fiber Netting Analysis
  - Algorithm for optimal dome shape with geodesic winding pattern (i.e., along iso-tensoids)
  - Algorithm for geodesic and hoop windings in cylindrical section
- Fatigue Analysis of Type 3 Tanks
  - Algorithm for residual compressive stresses introduced by auto-frettage, pre- and post-proof load distribution between liner and CF
  - Unloading of residual stresses under cryogenic conditions
  - S/N curves for Al 6061-T6 alloy, non-zero mean stresses
  - 5500 pressure cycles at 1.25 NWP (SAE J2579)
- Dynamic models for gaseous/liquid refueling, discharge, dormancy
- Models for off-board analysis
  - FCHtool and GREET for greenhouse gas emissions
  - H2A for pathway analysis
  - HDSAM for scenario analysis

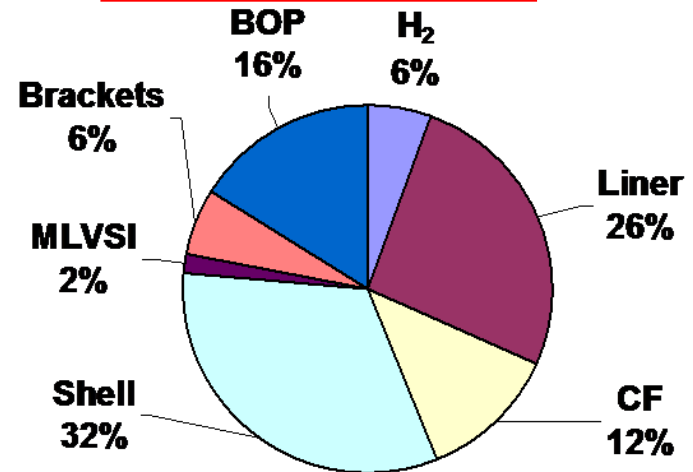


# Gravimetric and Volumetric Capacities

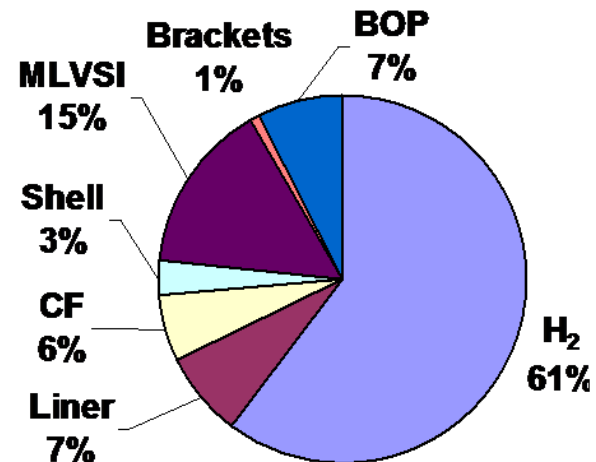
- 5.6-kg system meets 2015 targets
  - Gravimetric capacity > 9% with aluminum shell but higher cost
  - Maximum CF load share limited to 85% at cryogenic T, 276 bar
  - Liner heavier than CF
  - Insulation accounts for 15% of total volume



Weight Distribution



Volume Distribution

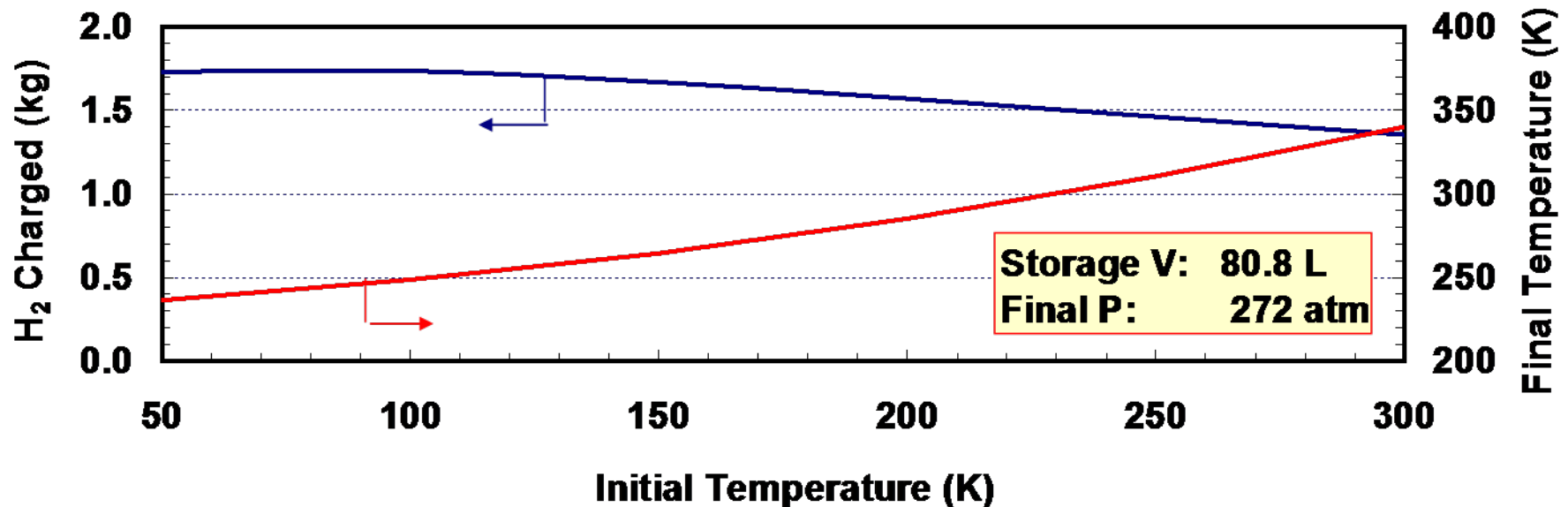


5.6-kg Recoverable H<sub>2</sub> System

# Storage Capacity: Compressed Hydrogen Option

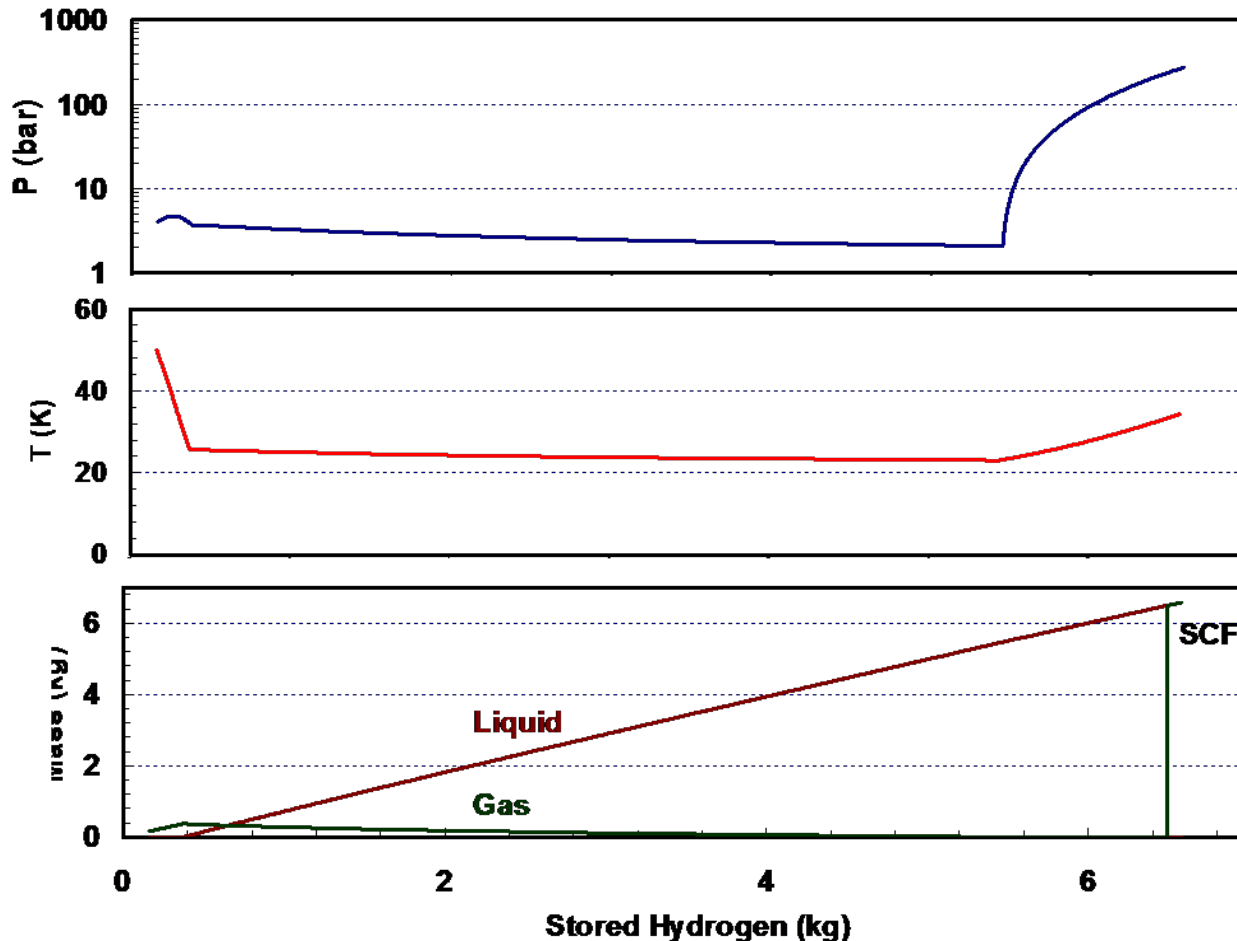
Refueling with compressed H<sub>2</sub> at 300 K

- Adiabatic refueling assuming that liner, CF and gas are isothermal during refueling (maximum possible capacity)
- Tank refueled to 272-atm (4000 psi) peak pressure
- 4 atm initial pressure, variable initial temperature
- Additional storage capacity with pre-cooled H<sub>2</sub> and refueling to higher than design pressure



# Refueling with LH2: Cryo-compressed Option

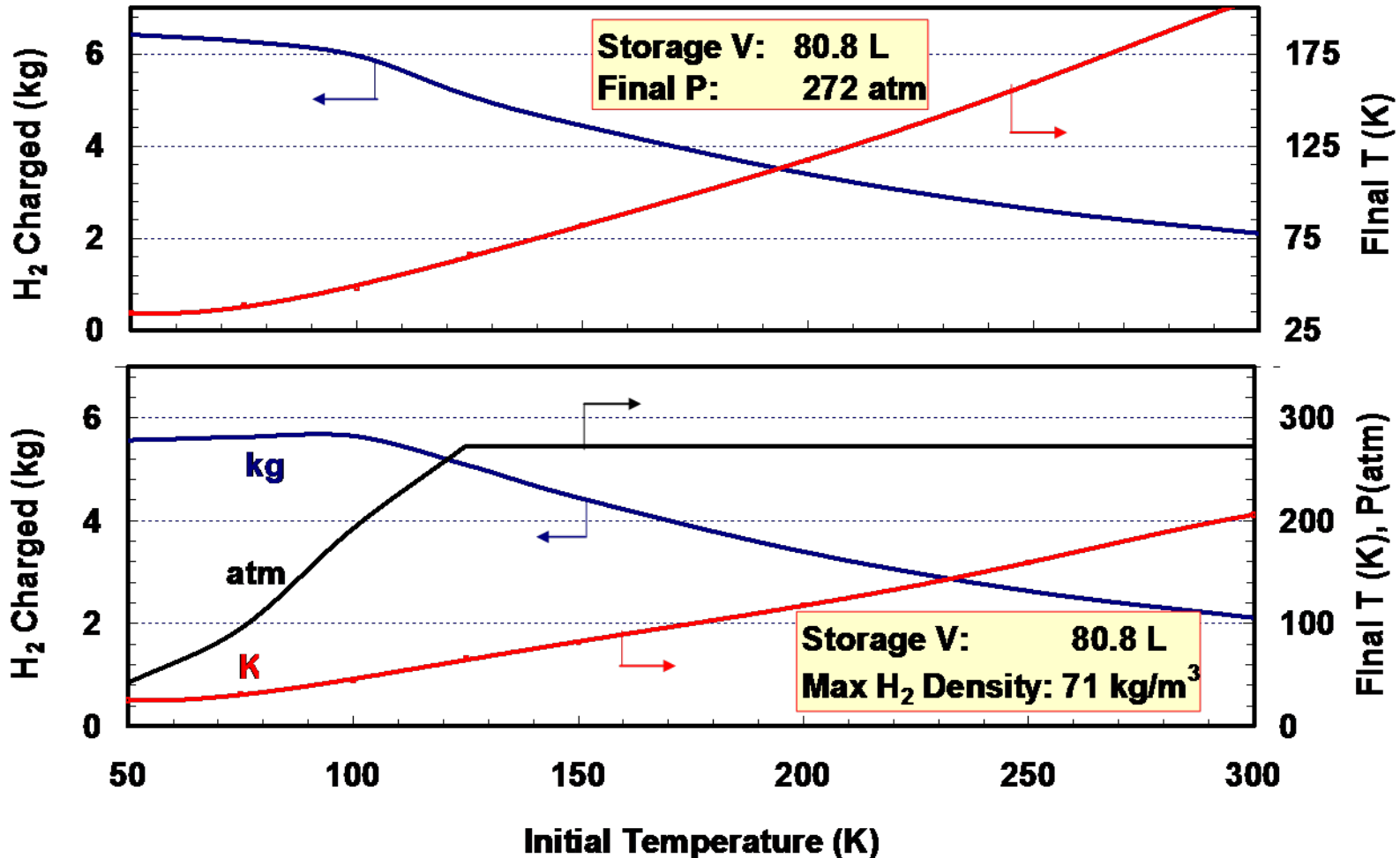
- Refueling with high-pressure LH<sub>2</sub> pump at 25% above tank pressure
- Storage capacity function of final pressure, 5.7 kg for P = 37.7 atm
- Depending on initial T and H<sub>2</sub> charged, final P may be less than 4 atm



- Initial conditions  
P=4 atm, T=50 K
- Gas  
m < 0.4 kg
- 2-Phase  
0.4 < m < 5.4 kg
- Sub-cooled Liquid  
5.4 < m < 6.5 kg
- Supercritical Fluid  
m > 6.5 kg

# Storage Capacity: Cryo-compressed Option

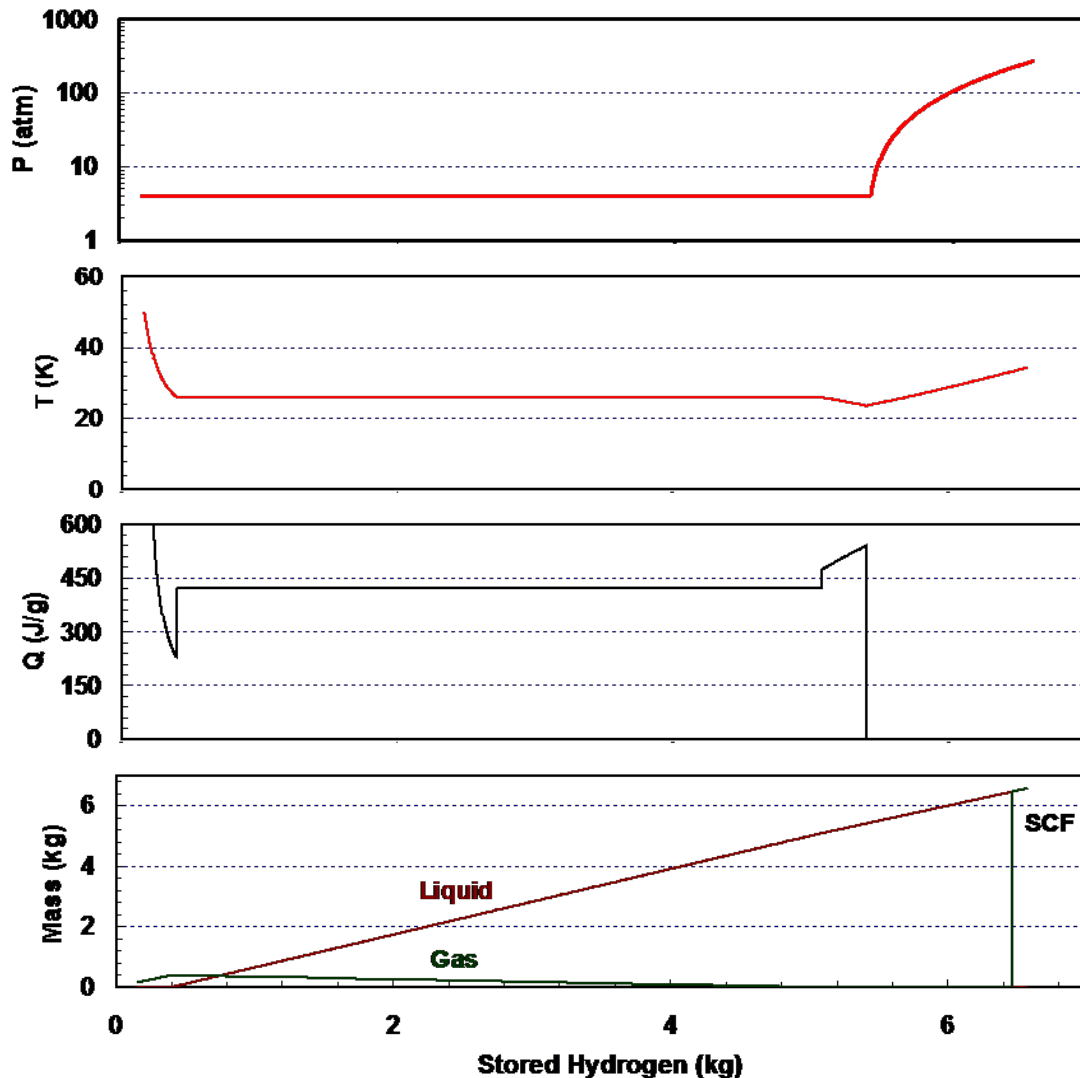
- Storage capacity is a function of initial temperature
  - 6.4 kg recoverable for initial  $T = 50$  K,  $P = 4$  atm





# Discharge Dynamics: Cryo-compressed Option

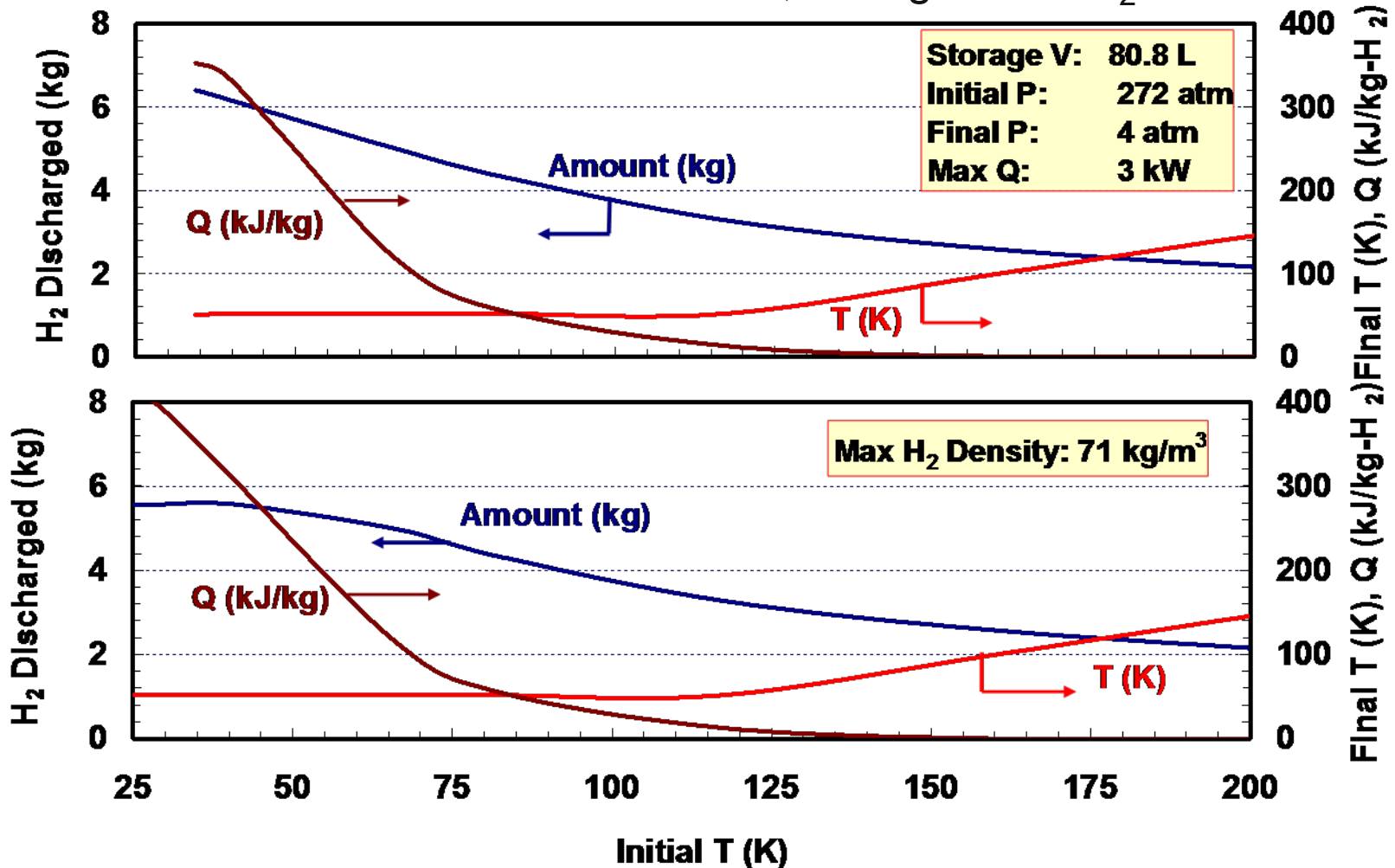
- Heat supplied to maintain 4-atm minimum delivery pressure



- Initial conditions:
  - $P = 272$  atm
  - $T = 34.3$  K
  - $m = 6.6$  kg
- 1.6 g/s full flow rate of  $H_2$
- Max  $Q = 3$  kW

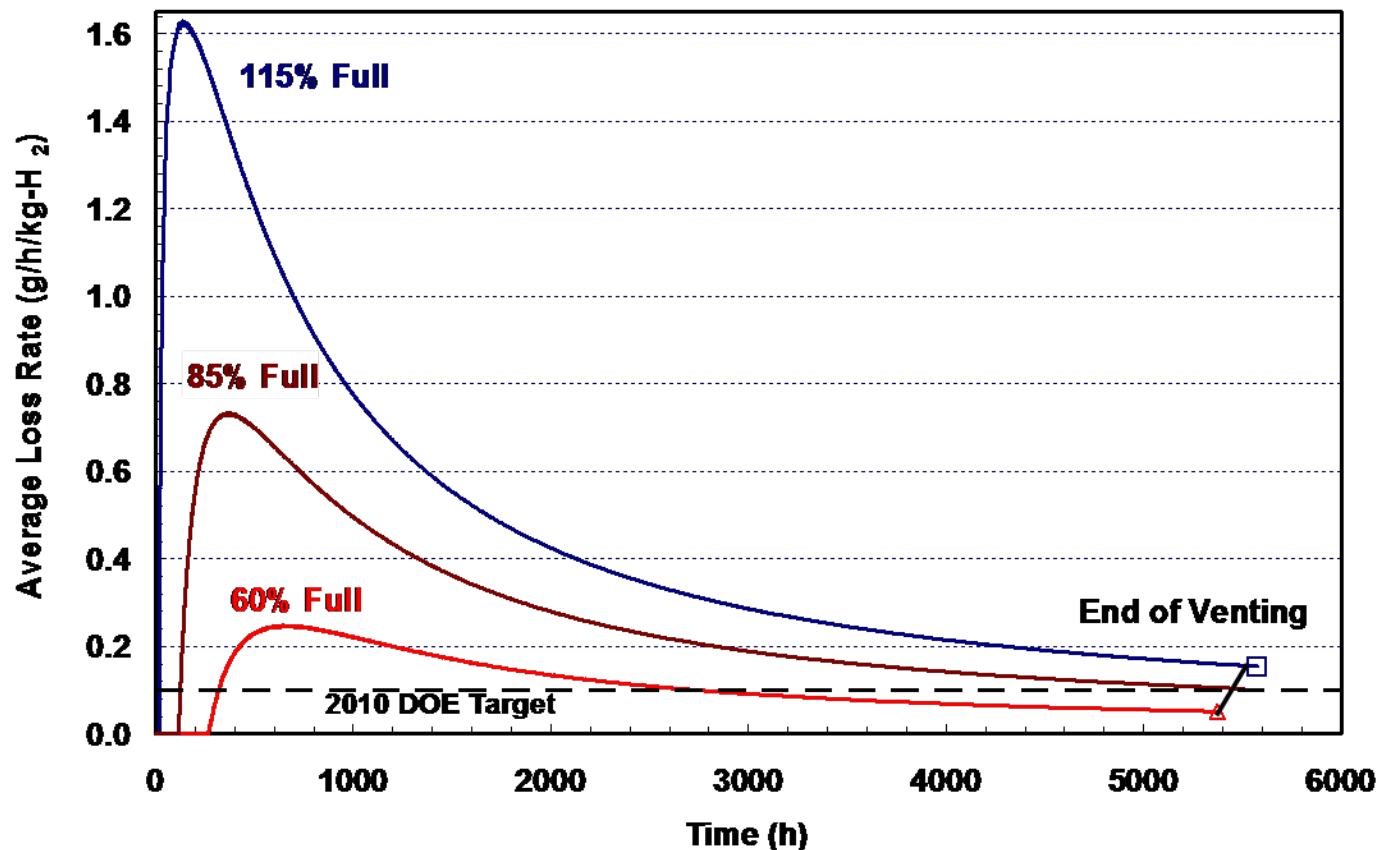
# Discharge Behavior: Cryo-compressed Option

- Total heat load is a function of initial temperature
  - 2.3 MJ for 34.3 K initial T, 6.4 kg stored H<sub>2</sub>



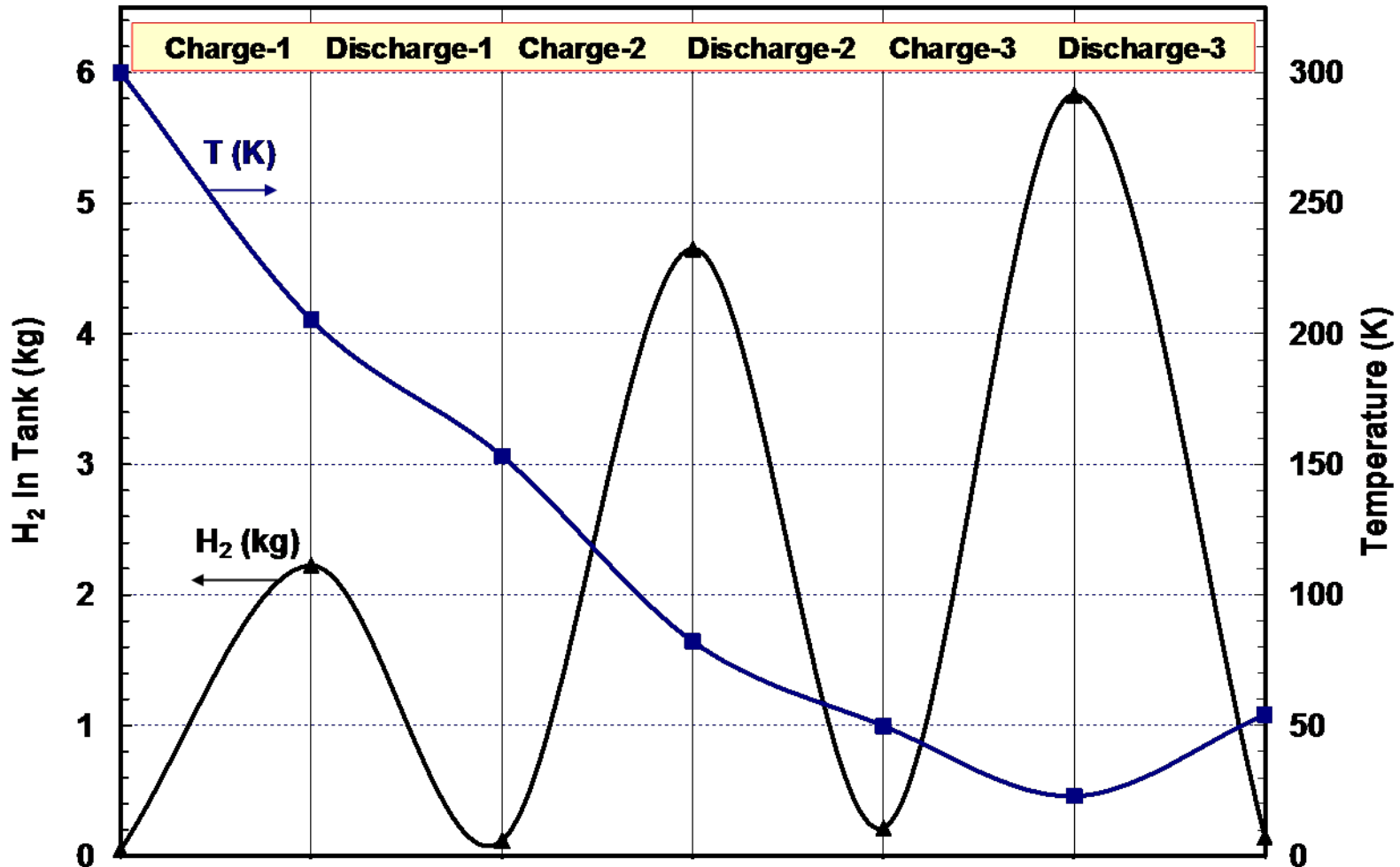
# Dormancy and Hydrogen Loss Rate

- No loss of hydrogen after tank reaches 323 K, tank 30% full
- Difficult to always meet the targets of 0.1/0.05 g/h/kg-H<sub>2</sub> with 5 W reference heat in-leakage rate
- No H<sub>2</sub> loss with minimal daily driving (LLNL paper)



# CH<sub>2</sub> to cCH<sub>2</sub> Transition

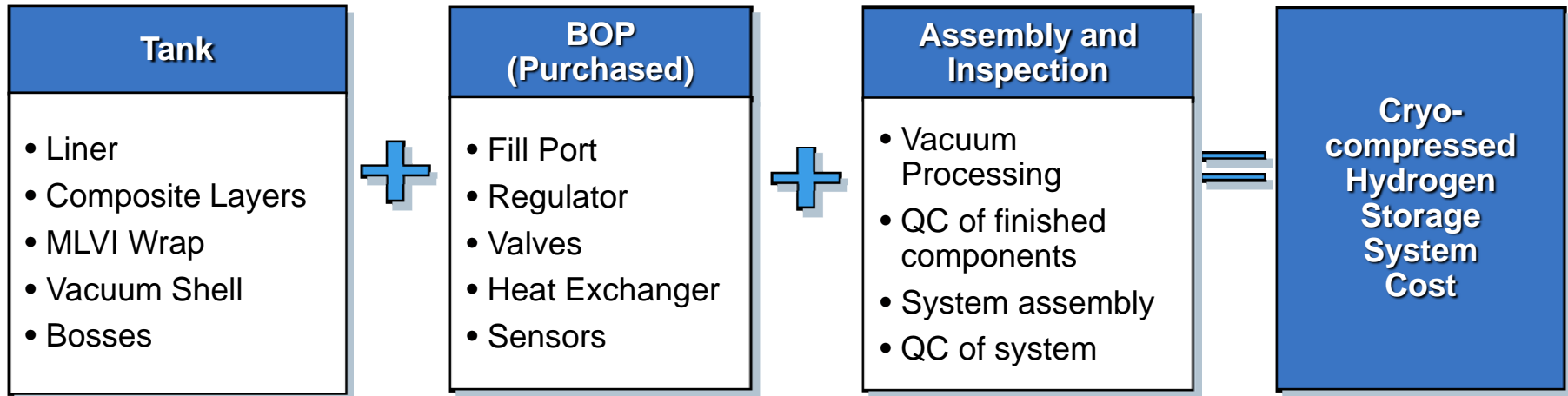
- Three complete charge-discharge cycles needed to reach 71 kg/m<sup>3</sup> hydrogen density



**The high volume (500,000 units/year) manufactured cost for all H<sub>2</sub> storage systems is estimated from raw material prices, capital equipment, labor, and other operating costs.**

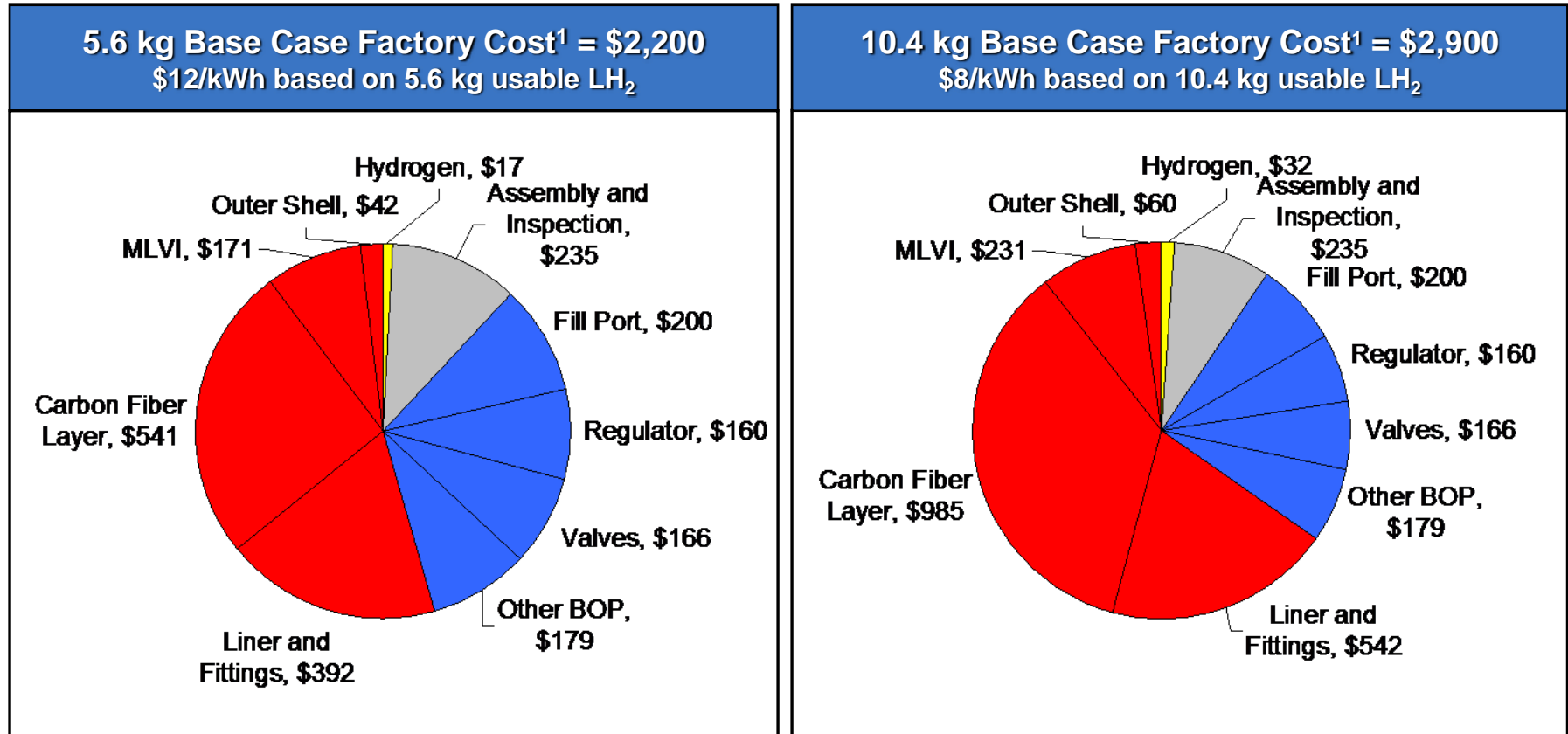
### BOP Bottom-up Costing Methodology

- Develop Bill of Materials (BOM)
- Obtain raw material prices from potential suppliers
- Develop production process flow chart for key subsystems and components
- Estimate manufacturing costs using TIAX cost models (capital equipment, raw material price, labor rates)



**We modeled material and manufacturing process costs for the cryo-compressed tank, while the BOP is assumed to be purchased.**

The carbon fiber layer is the most expensive single component and accounts for about 25% and 35% of the base case 5.6 and 10.4 kg systems costs.



<sup>1</sup> Cost estimate in 2005 USD. Includes processing costs.

The BOP components account for about 30% and 25% of the base case 5.6 and 10.4 kg system costs, respectively.

# WTT Efficiency

- WTT efficiency = 41.1% (LH<sub>2</sub> refueling)
- Assumptions

Process/Process Fuels	Nominal Value	Source/Comment
Electricity production	32.2% thermal efficiency	EIA projected U.S. grid for 2015, inclusive of 8% transmission loss from power plant to user site
North American natural gas production	93.5% efficiency	GREET data
H <sub>2</sub> production by SMR	73% efficiency	H2A
H <sub>2</sub> Liquefaction	8.2 kWh/kg	HDSAM, 150 tons/day liquefier
Liquid H <sub>2</sub> (LH <sub>2</sub> ) delivery by truck	284 km round trip	HDSAM
Truck capacity	4300 kg	HDSAM
Boil-off losses	9.5%	HDSAM: liquefaction 0.5%, storage 0.25%/day, loading 0.5 %, unloading 2%, cryopump 3%
Vehicle refueling with LH <sub>2</sub>	2 kg/min; 80% isentropic efficiency	BMW LH <sub>2</sub> pump data
Greenhouse gas emissions	range	Emission factors data from GREET

# Off-Board Cost and Performance Summary

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- Hydrogen production cost is dominated by fuel cost
  - Central SMR ~ \$1.6/kg (77% fuel, 14% capital)
  - Central electrolysis ~ \$3.8/kg (6 cents/kWh, 80% fuel, 15% capital)
- Hydrogen delivery cost is dominated by capital cost
  - ~ \$6.1/kg for 2% market (60% capital, 10% fuel)
  - ~ \$3.2/kg for > 15% market (55% capital, 18% fuel)
- Ownership cost
  - ~12 - 17 cents/mile (15%/2% market) for NG/standard grid scenario
  - ~16 - 21 cents/mile (15%/2% market) for electrolysis/renewable
  - ~10 cents/mile for conventional gasoline ICEV (\$3/gal untaxed)
- WTT efficiency: 36 - 41%
- GHG emissions
  - ~ 0.31 - 0.37 kg/mile for NG/standard grid scenario
  - ~ 0 kg/mile for electrolysis/renewable scenario
  - ~ 0.35 kg/mile for gasoline ICEV (31 mpg fuel economy)



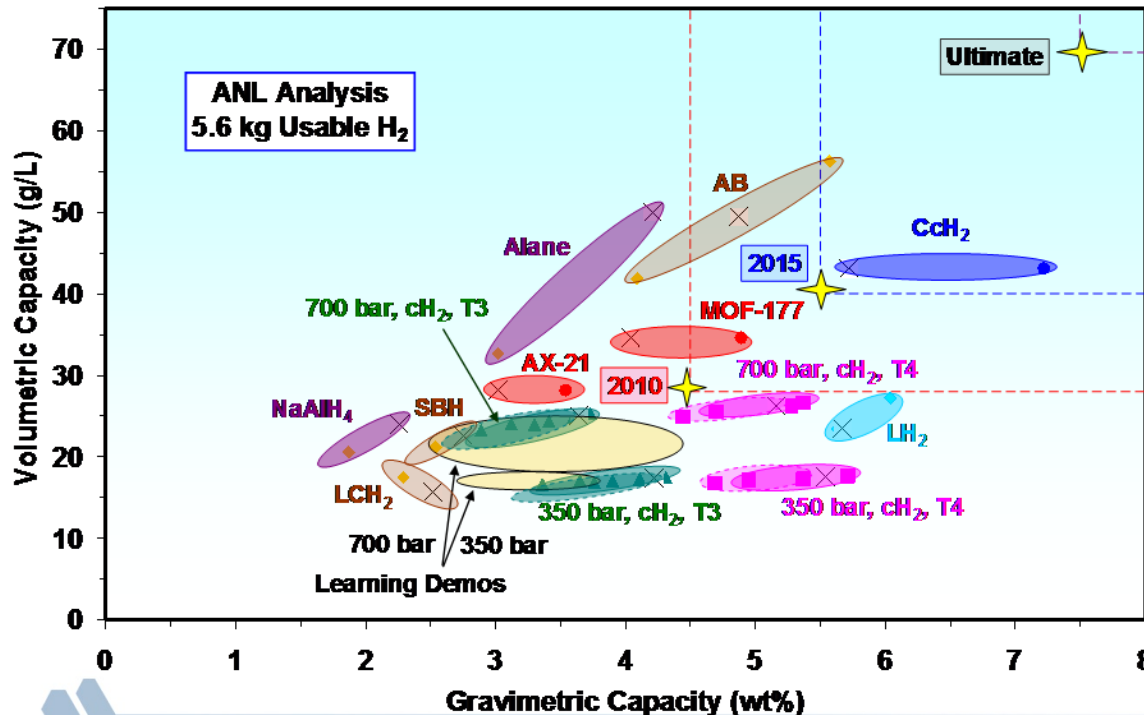
# Summary and Conclusions

- Cryo-compressed: 71 kg/m<sup>3</sup> max density or 272 atm max pressure
- Results given as single data points, consult references for range, sensitivity and background
- Metrics cover all DOE targets for on-board and off-board storage
- Some results vetted, others for developmental materials and processes

Performance and Cost Metric	Units	cH2 350-T4	cH2 700-T4	LH2	CcH2	MOF-177	2010 Targets	2015 Targets	Ultimate Targets
<b>Tank</b>		<b>1-Tank</b>	<b>1-Tank</b>						
Usable Storage Capacity (Nominal)	kg-H <sub>2</sub>	5.6	5.6	5.6	5.6	5.6			
Usable Storage Capacity (Maximum)	kg-H <sub>2</sub>	5.6	5.6	5.6	6.6	5.6			
System Gravimetric Capacity	wt%	5.5	5.2	5.6	5.5-9.2	4.0	4.5	5.5	7.5
System Volumetric Capacity	kg-H <sub>2</sub> /m <sup>3</sup>	17.6	26.3	23.5	41.8-44.7	34.6	28	40	70
Storage System Cost	\$/kWh	15.5	18.9	TBD	12	18	4	2	TBD
Fuel Cost	\$/gge	4.2	4.3	TBD	4.80	4.6	2-3	2-3	2-3
Cycle Life (1/4 tank to Full)	Cycles	NA	NA	NA	5500	5500	1000	1500	1500
Minimum Delivery Pressure, FC/ICE	atm	4	4	4	3-4	4	4/35	3/35	3/35
System Fill Rate	kg-H <sub>2</sub> /min	1.5-2	1.5-2	1.5-2	1.5-2	1.5-2	1.2	1.5	2.0
Minimum Dormancy (Full Tank)	W-d	NA	NA	2	4-30	2.8			
H <sub>2</sub> Loss Rate (Maximum)	g/h/kg-H <sub>2</sub>	NA	NA	8	0.2-1.6	0.9	0.1	0.05	0.05
WTT Efficiency	%	56.5	54.2	22.3	41.1	41.1	60	60	60
GHG Emissions (CO <sub>2</sub> eq)	kg/kg-H <sub>2</sub>	14.0	14.8	TBD	19.7	19.7			
Ownership Cost	\$/mile	0.13	0.14	TBD	0.12	0.15			

# Storage Capacity

- Of all the systems built, Gen3 CcH<sub>2</sub> has the highest demonstrated gravimetric and volumetric capacity
- Alane slurry shows high volumetric capacity but stable 70-wt% slurry not formulated, volume-exchange tank not developed
- On-going studies to find AB/IL formulations that remain liquid under all conditions, volume-exchange tank not developed
- cH<sub>2</sub> model capacities in agreement with Tech Val data

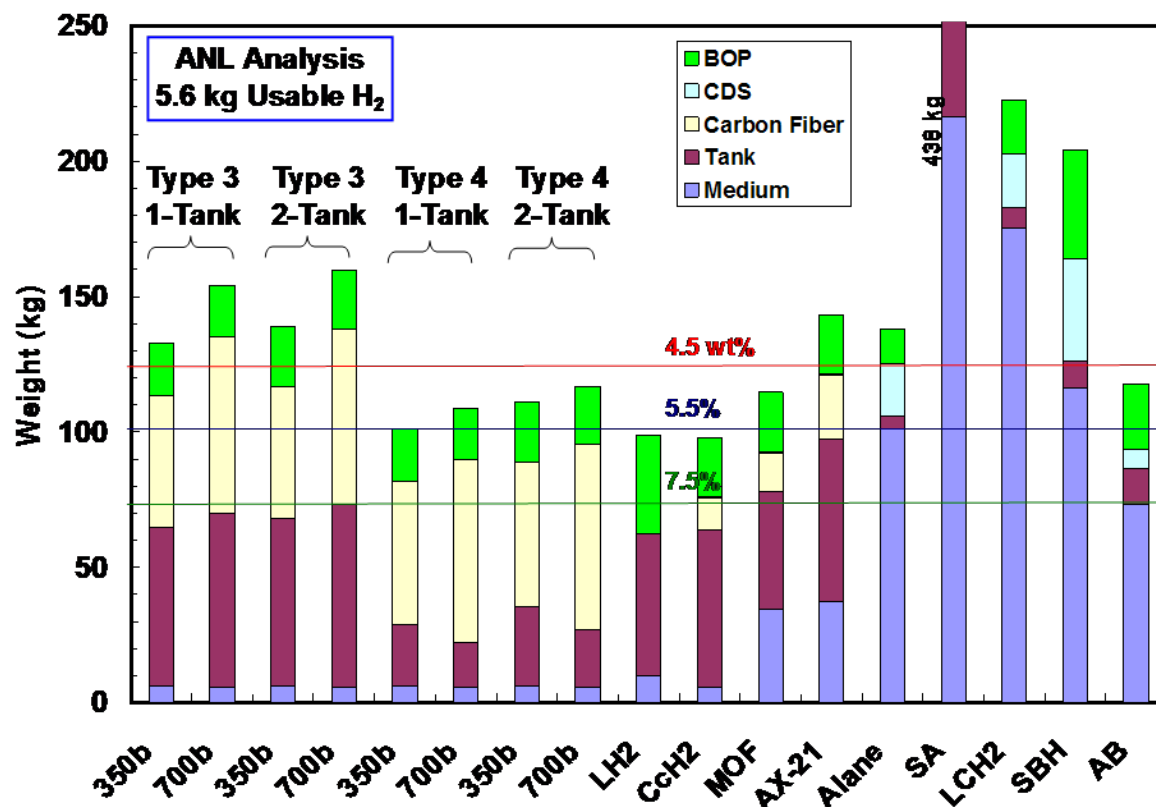


- Diagram to be regarded as a snapshot in time
- Different systems not analyzed to same level of sophistication
- Advanced materials not ready for deployment
- Some component concepts require further development

# Weight Distribution

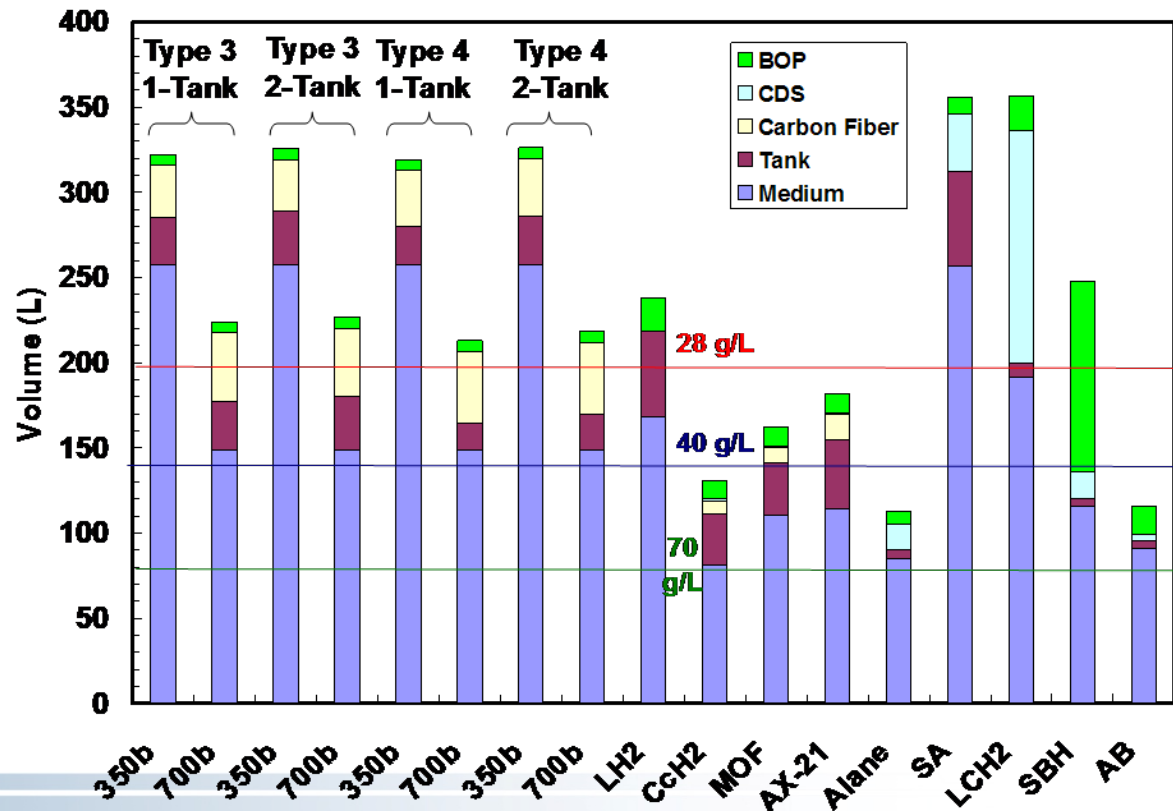
- 350-bar  $cH_2$ ,  $LH_2$  &  $CcH_2$  systems may meet 2015 gravimetric target
- $CcH_2$  system with Al shell approaches the ultimate gravimetric target
- CF is the main contributor to the overall weight in  $cH_2$  systems
- Metal liner is a heavy component in all Type-3 pressure vessels
- Medium weight dominates in metal hydride and chemical  $H_2$  systems

$cH_2$ : Compressed  $H_2$   
 350b: 350 bar  
 700b: 700 bar  
 $LH_2$ : Liquid  $H_2$   
 $CcH_2$ : Cryo-compressed  $H_2$   
 MOF: MOF-177  
 SA:  $TiCl_3$  catalyzed  $NaAlH_4$   
 LCH2: Organic liquid carrier  
 SBH: Alkaline  $NaBH_4$  solution  
 AB: Ammonia borane



# Volume Distribution

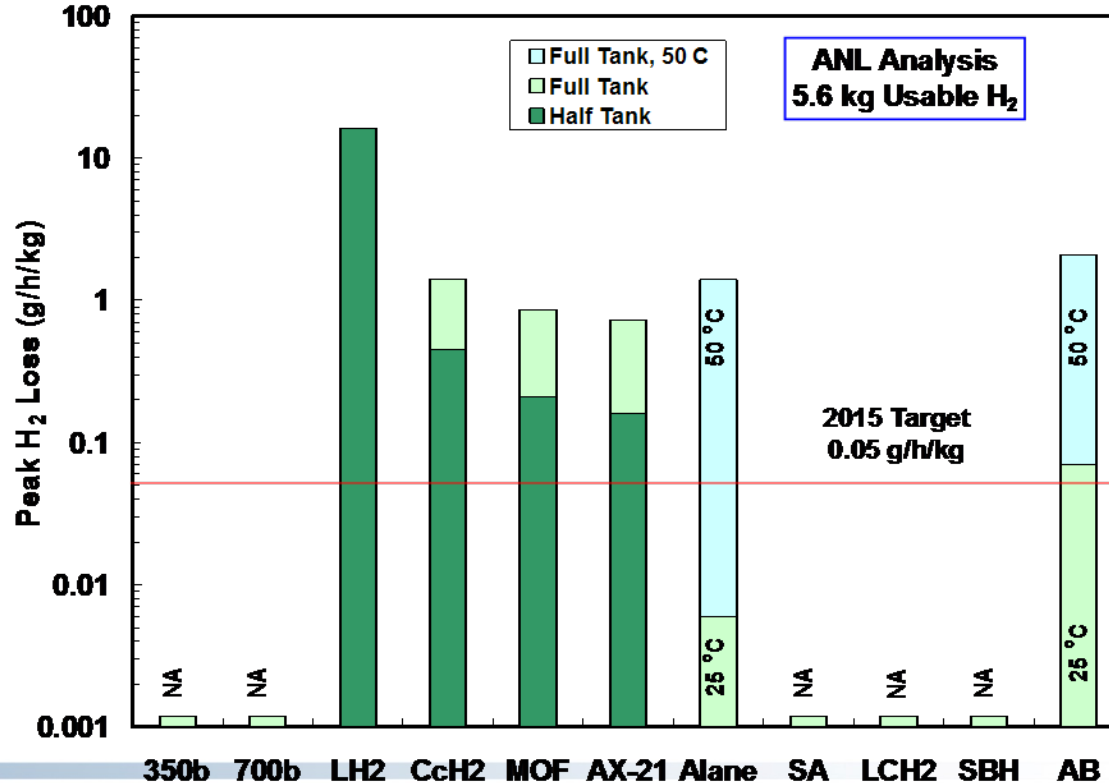
- CcH<sub>2</sub> system meets 2015 volumetric target but not ultimate target
- Medium volume significant in all options and, by itself, exceeds the 2015 system target in cH<sub>2</sub> systems
- Insulation volume important in cryogenic systems
- CDS in LCH<sub>2</sub> is bulky because of highly endothermic reaction
- BOP in SBH (adiabatic reactor, exothermic release) is bulky because of condensers



BOP: Balance of Plant  
 CDS: Charge-Discharge System

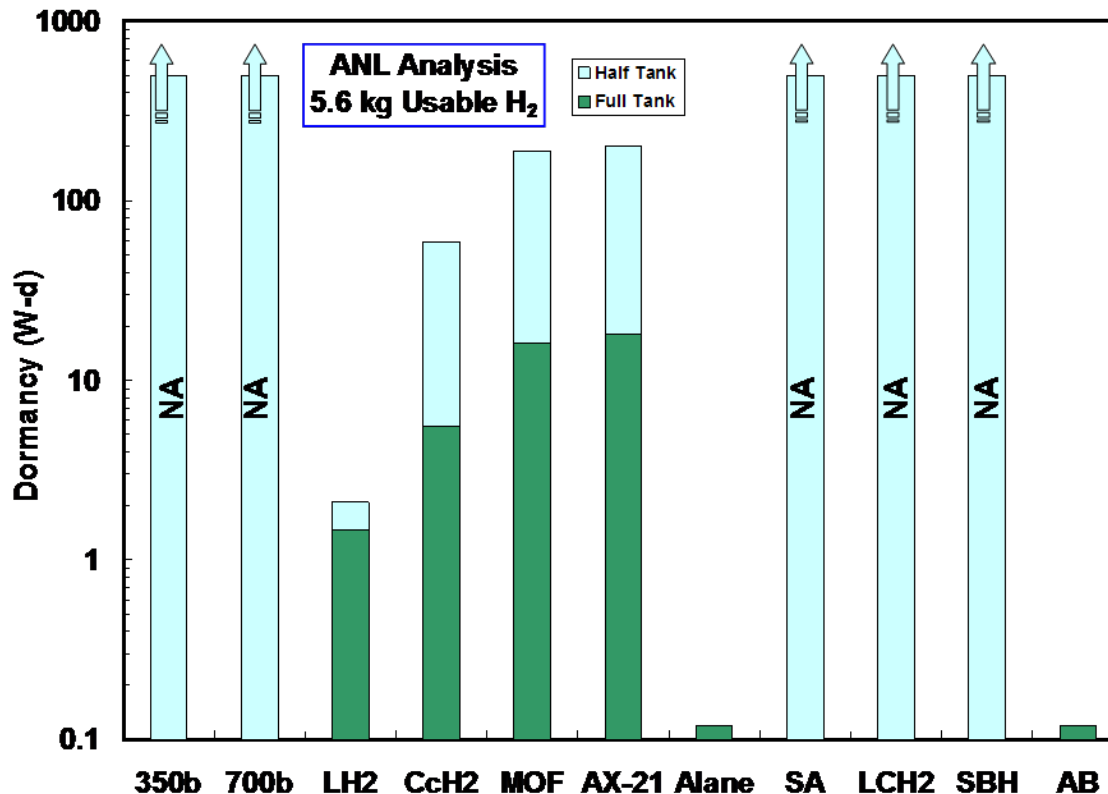
# Hydrogen Loss During Extended Parking

- 40% of H<sub>2</sub> stored in LH<sub>2</sub> tank vented to ambient in a typical use cycle
- Negligible H<sub>2</sub> loss from insulated cryogenic pressure vessels with some daily driving
- H<sub>2</sub> loss from alane determined by kinetics and ambient temperature, not by heat transfer
- H<sub>2</sub> loss from AB/IL determined by kinetics, ambient temperature, and heat transfer coefficient



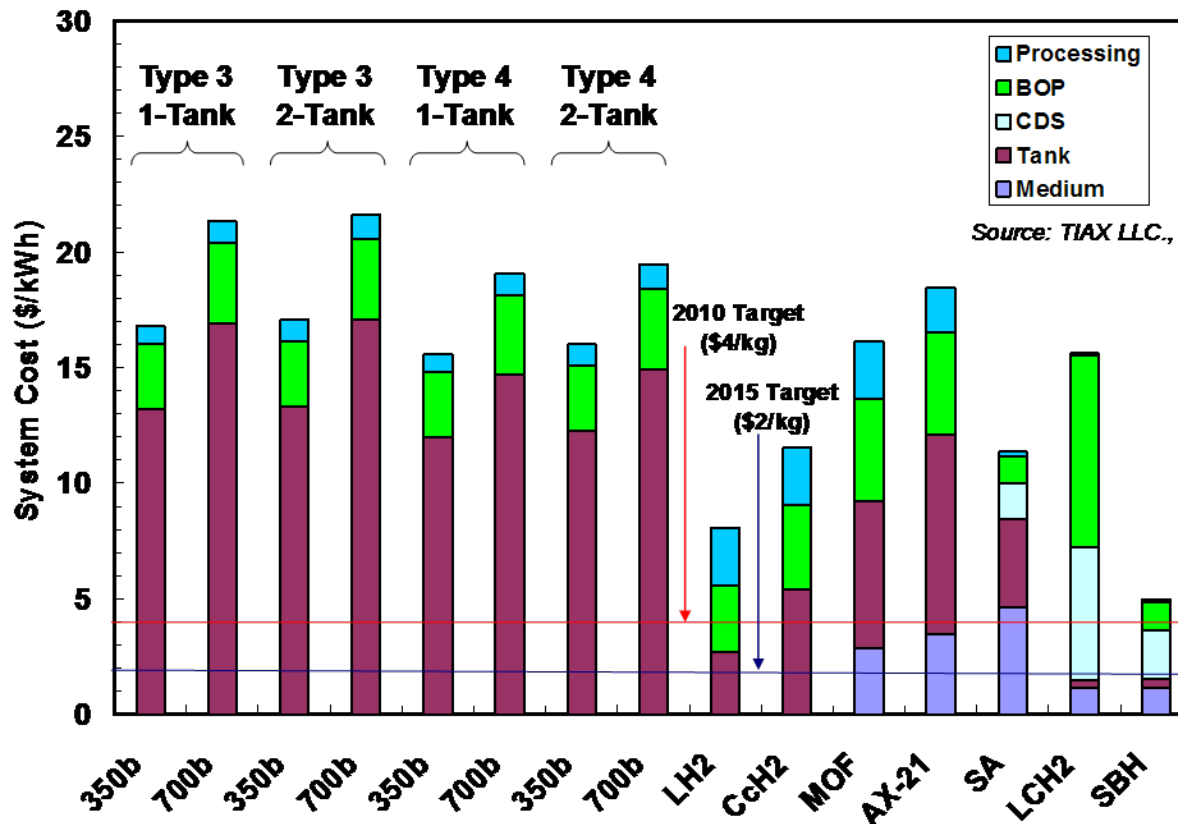
# Dormancy

- Shorter dormancy in LH<sub>2</sub> system if the fuel tank is partially full
- Longer dormancy in CcH<sub>2</sub> system with partially-full tank, no stranded driver syndrome
- Longer dormancy in cryogenic sorbent systems than CcH<sub>2</sub> because of heat of desorption
- Dormancy definition not meaningful for alane and AB storage



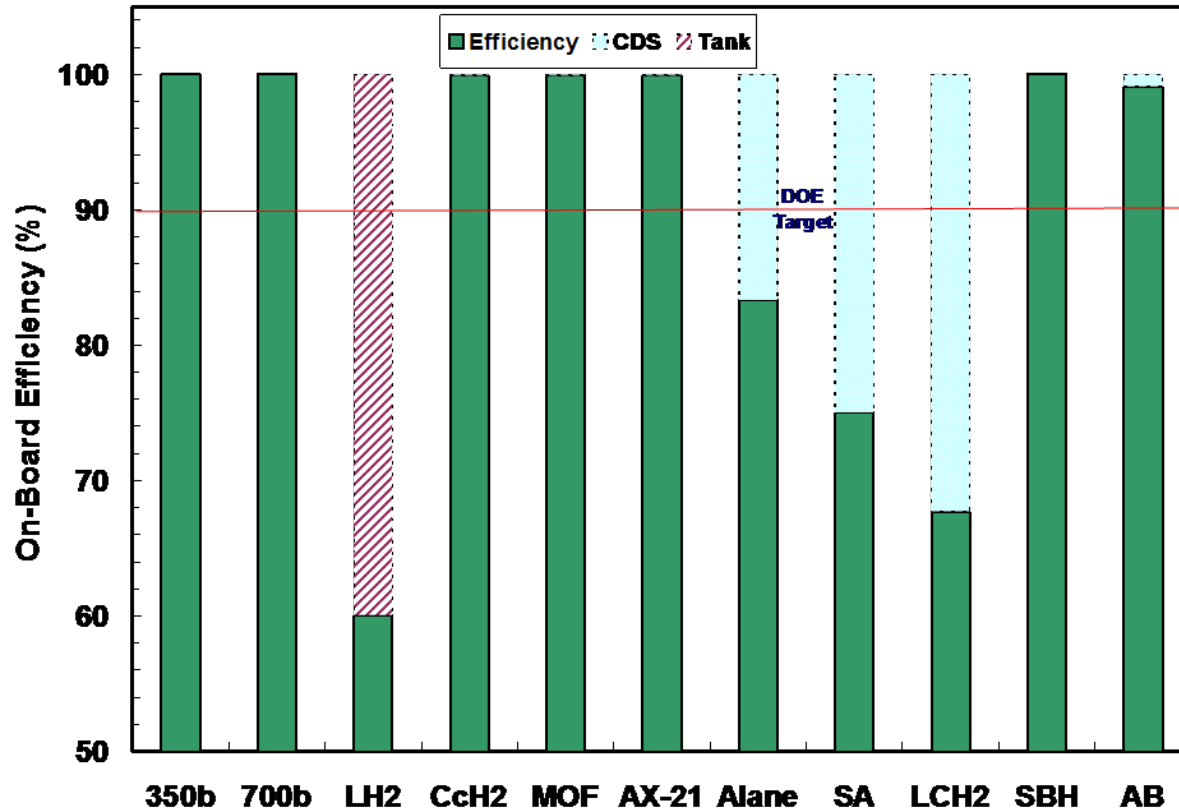
# Cost of On-Board Systems at High-Volume Manufacturing

- Cost data from TIAX studies with ANL inputs, 500,000 units/year
- Fiber cost dominates in  $\text{CH}_2$  systems, less expensive in cryogenic sorption systems
- Material cost important in sorption systems and in SA system
- Dehydrogenation catalyst cost important in LCH<sub>2</sub> system



# Efficiency of On-Board Systems

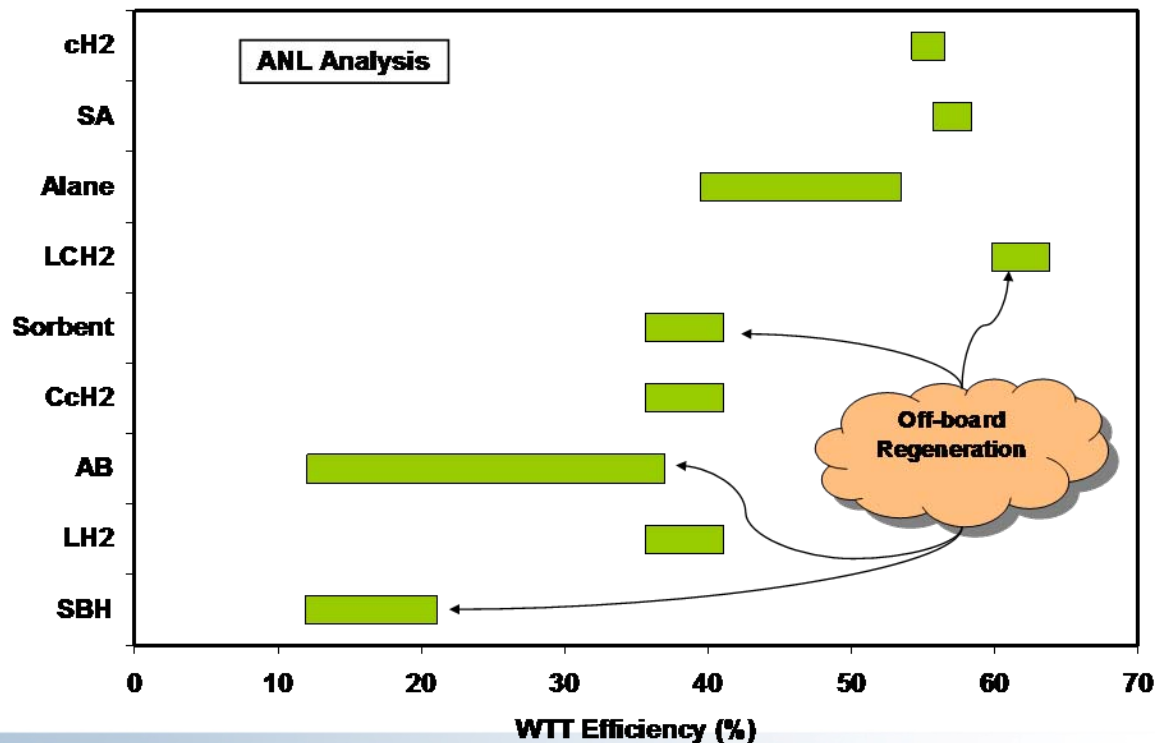
- Venting loss accounts for inefficiency of LH<sub>2</sub> system
- 10-30% H<sub>2</sub> consumed in alane, SA and LCH<sub>2</sub> systems to sustain high-temperature endothermic reactions
- ~1% loss in AB system efficiency because of fuel pump, additional FCS coolant and radiator fan power
- DOE target for on-board system efficiency is 90%





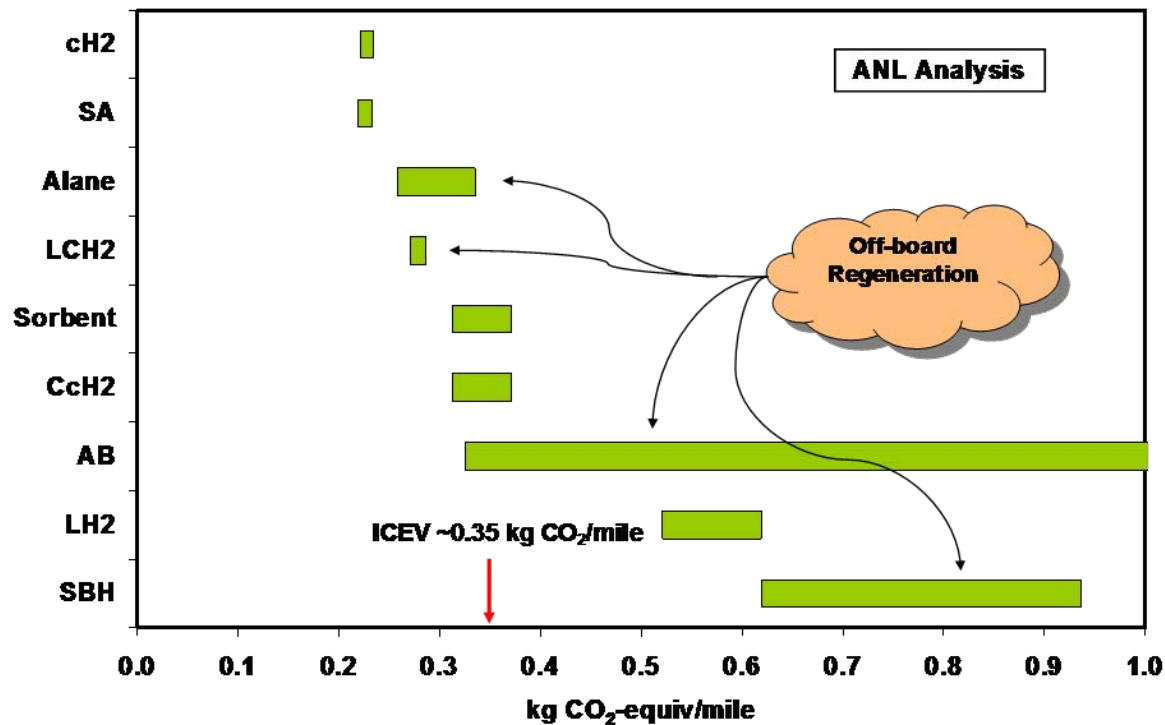
# Well-to-Tank Efficiency

- 350- and 700-bar  $\text{CH}_2$  options have <60% WTT efficiency
- Reversible metal hydrides may have higher WTT efficiency than  $\text{CH}_2$
- $\text{LCH}_2$  regeneration is exothermic and can reach 60% efficiency
- High uncertainty in alane regeneration efficiency because of vacuum distillation steps and low-grade waste heat requirement
- Options involving cryogenic  $\text{H}_2$  have < 41% WTT efficiencies
- Low efficiencies for AB and SBH regeneration



# Greenhouse Gas Emissions

- Values given in kg of CO<sub>2</sub> equivalent per kg of H<sub>2</sub> delivered to the vehicle or per mile driven
  - 63.4 mpgge assumed fuel economy for 2015 advanced FC vehicle
- As reference, GHG emissions for 2015 mid-size ICE vehicle with 31 mpgge fuel economy is 0.35 kg-CO<sub>2</sub>/mile



# Refueling Cost

- H2A data for cost of unit operations, natural gas at \$0.22/Nm<sup>3</sup>
- Liquefaction contributes significantly to the fuel cost in options requiring LH<sub>2</sub>
- Regeneration is the main component of fuel cost in SBH option
- No storage option can meet the \$2-3/kg cost target (untaxed)

